

Integration of Xantrex HY-100 Hybrid Inverter with an AC Induction Wind Turbine

D. Corbus, C. Newcomb, S. Friedly



NREL

National Renewable Energy Laboratory

1617 Cole Boulevard
Golden, Colorado 80401-3393

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Contract No. DE-AC36-99-GO10337

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Prepared under Task No. IG135000



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1.0 Table of Contents

1.0	Table of Contents	1
2.0	Table of Tables	2
3.0	Table of Figures.....	2
4.0	Disclaimer.....	3
5.0	Background of Wind-Diesel Inverters.....	3
6.0	Project Approach	3
7.0	Modeling Approach.....	4
8.0	Inverter Development.....	4
8.1	Inverter Description	4
8.2	Control Algorithms	6
9.0	Testing of the Modified Inverter	8
9.1	Hybrid Power Test Bed.....	8
9.2	Test Procedure	10
9.3	Functionality Checks	10
9.4	Test Results with AC Source Simulator	10
9.5	Testing with the AOC 15/50 Wind Turbine	10
10.0	Summary of Inverter Testing.....	11
Appendix A:	Xantrex HY-100 Inverter Description	12
	Inverter/Rectifier Bridge.....	12
	Generator Interface	12
	Battery Charge Controller.....	12
	Operator Interface	13
	Control States.....	13
	Inverter State	13
	Generator Support State	13
	Equalize State.....	13
	Generator Only State.....	14
	Blackout State	14
	Inverter/Rectifier Bridge Control.....	14
	Battery Charge Controller Control.....	14
	Generator Interface Control	14
	Instrumentation	15
	Self-Protection, Fault Detection, and Alarms	15
	Performance Specifications	16
Appendix B:	MATLAB Dynamic and Transient Wind-Diesel Models.....	17
Appendix C:	Inverter Test Results	78
	Functionality Checks	78
1.1	Test Results with AC Source Simulator	80
1.1.1	Test: Village Load Step Changes: Adding Load.....	80
1.1.2	Test: Village Load Step Changes: Decreasing Load.....	81
1.1.3	Test: Wind Turbine Trip Offline: Diesel Generator On.....	82
1.1.4	Test: Wind Turbine Trip Offline: Diesel Generator Off	83
1.1.5	Test: Battery Charging	83
1.1.6	Test: State Transition from Inverter to Charge and from Charge to Inverter.....	85
1.1.7	Test: Transition to Shutdown on Inverter Fault	88
1.2	Testing with the AOC 15/50 Wind Turbine.....	88
1.2.1	Test: Wind Turbine Startup at High Power with Diesel	88
1.2.2	AOC 15/50 Soft Start Mode Start Up	89

Appendix D: A Preliminary Description of Parallel Operation of the Inverter with a Diesel Genset	90
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2.0 Table of Tables

Table 1. Inverter Settings	78
Table 2. Functionality Checks Performed	79

3.0 Table of Figures

Figure 1. State transition line diagram.	5
Figure 2. Wind-diesel hybrid system schematic.....	6
Figure 3. Dispatch matrix zones.....	7
Figure 4. Top-level dispatch logic.....	8
Figure 5. Hybrid Power Test Bed (HPTB) configuration.	9
Figure 6. Village load (kW).....	80
Figure 7. Village load (kW).....	81
Figure 8. Battery voltage (V).	84
Figure 9. Village load (kW).	84
Figure 10. AC SIM power (kW).	84
Figure 11. Genset power (kW).....	84
Figure 12. Inverter power (kW).	85
Figure 13. Dump load power (kW).....	85
Figure 14. Battery voltage (V).	85
Figure 15. Village load (kW).....	85
Figure 16. AC SIM power (kW).	86
Figure 17. Genset power (kW).	86
Figure 18. Inverter power (kW).	86
Figure 19. Dump load power (kW).....	86
Figure 20. DC bus voltage (V).	87
Figure 21. Village load (kW).....	87
Figure 22. AC SIM power (kW).	87
Figure 23. Genset power (kW).	87
Figure 24. Inverter power (kW).	87
Figure 25. Dump load power (kW).....	87

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5.0 Background of Wind-Diesel Inverters

Wind-diesel systems have been used for remote power for many years in various configurations. Most of the wind-diesel systems to date have been based on a system design that uses small wind turbines (1-10 kilowatts, or kW) connected to a DC bus. These systems can use inverter controllers that are designed for photovoltaic (PV) systems because the inverter design is similar for the two technologies. However, larger AC wind turbines (50-150 kW) are significantly cheaper than small DC wind turbines (and much cheaper than PV systems) on an installed-kilowatt basis and are better matched to many remote off-grid energy requirements, such as village electrification. Because of these advantages, the use of larger wind turbines in wind-diesel systems is advantageous.

Converters are a key component in hybrid power systems. To date, wind-diesel hybrid power systems in the 50-150 kW size range have relied on rotary converters (i.e., a DC machine coupled directly to an AC synchronous generator) for power conversion. These systems are cheaper and have been more easily maintained in remote areas. However, these systems operate at lower efficiencies than solid-state inverters. The recent advances in power electronics in the past decade and the subsequent reduction in cost and increase in reliability make solid-state inverters a logical converter option for future wind-diesel systems.

6.0 Project Approach

Several issues must be addressed before solid-state inverters can be used in wind-diesel systems with larger wind turbines. This project addresses those issues by using a commercial hybrid inverter designed for PV-diesel systems and modifying the inverter for use with an AC induction wind turbine. Another approach would have entailed building an inverter specifically for use with an AC induction wind turbine, but that was beyond the scope of this project.

The inverter chosen for this project was a Xantrex HY-100, an inverter designed for PV systems. The unit consists of an inverter/rectifier bridge, a generator interface contactor, a battery charge controller, a hybrid controller, and the associated control electronics. Details of the inverter may be found in Appendix A.

A twofold approach was taken to integrating the existing inverter for use with an AC induction wind turbine: 1) development of a detailed model to model both steady-state and transient behavior of the system, and 2) modification and testing of the inverter with an induction wind turbine based on the modeling results. This report describes these two tasks.

7.0 Modeling Approach

Two models were written for the wind-diesel inverter system, the MATLAB NREL Modified Inverter Dynamic Model and the Modified Inverter Transient Model. The models were developed by Xantrex (formerly Trace Technologies) and NREL to model the system with an induction wind turbine and a dump load and to determine any needed modifications to the system controller.

The dynamic model is based on an energy balance among a wind turbine, inverter/battery, diesel generator, grid load, and dump load. Logic for transitioning between states is computed by the MATRIX logic function (see Appendix B for a complete model description). The MATRIX uses filtered/averaged values for battery state of charge (SOC) and net load demand to determine which operating state should be requested. The battery's SOC is related to the battery's voltage and the grid's net load demand and is defined as grid load minus wind turbine output in kilowatts.

The transient model uses a MATLAB Simulink program to model the various system components and characterize the transient response of the system to variables such as voltage and frequency response to large shifts in dump load or grid power. A detailed description of the model may be found in Appendix B.

8.0 Inverter Development

8.1 Inverter Description

The inverter may operate with a diesel generator (as a current source) or in stand-alone mode (as a voltage source), and it can charge batteries with the diesel generator or excess energy from the wind turbine generator, which in this case is an Atlantic Orient Corporation (AOC) 15/50 wind turbine or a 65-kW wind turbine simulator. The inverter is able to instantaneously control power flows between the AC and DC bus. A state diagram of the inverter developed by Xantrex technologies is shown in Figure 1.

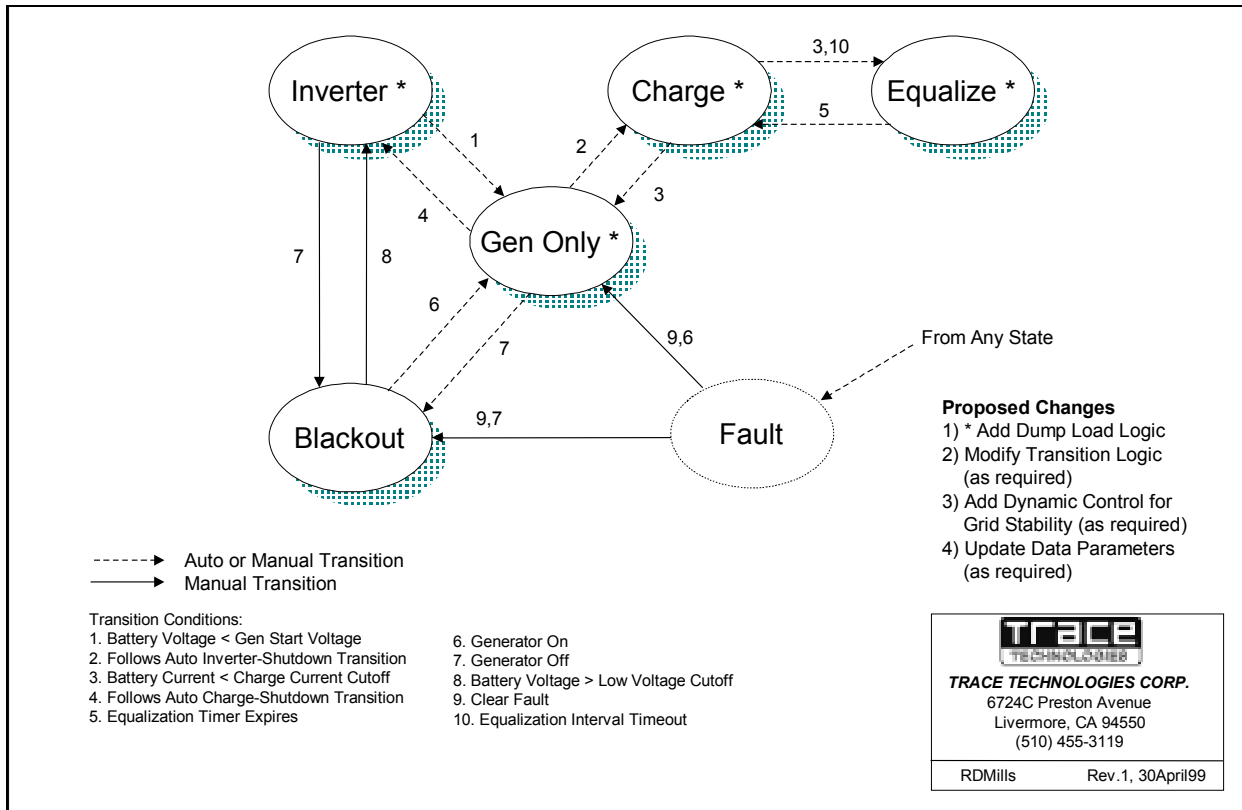


Figure 1. State transition line diagram.

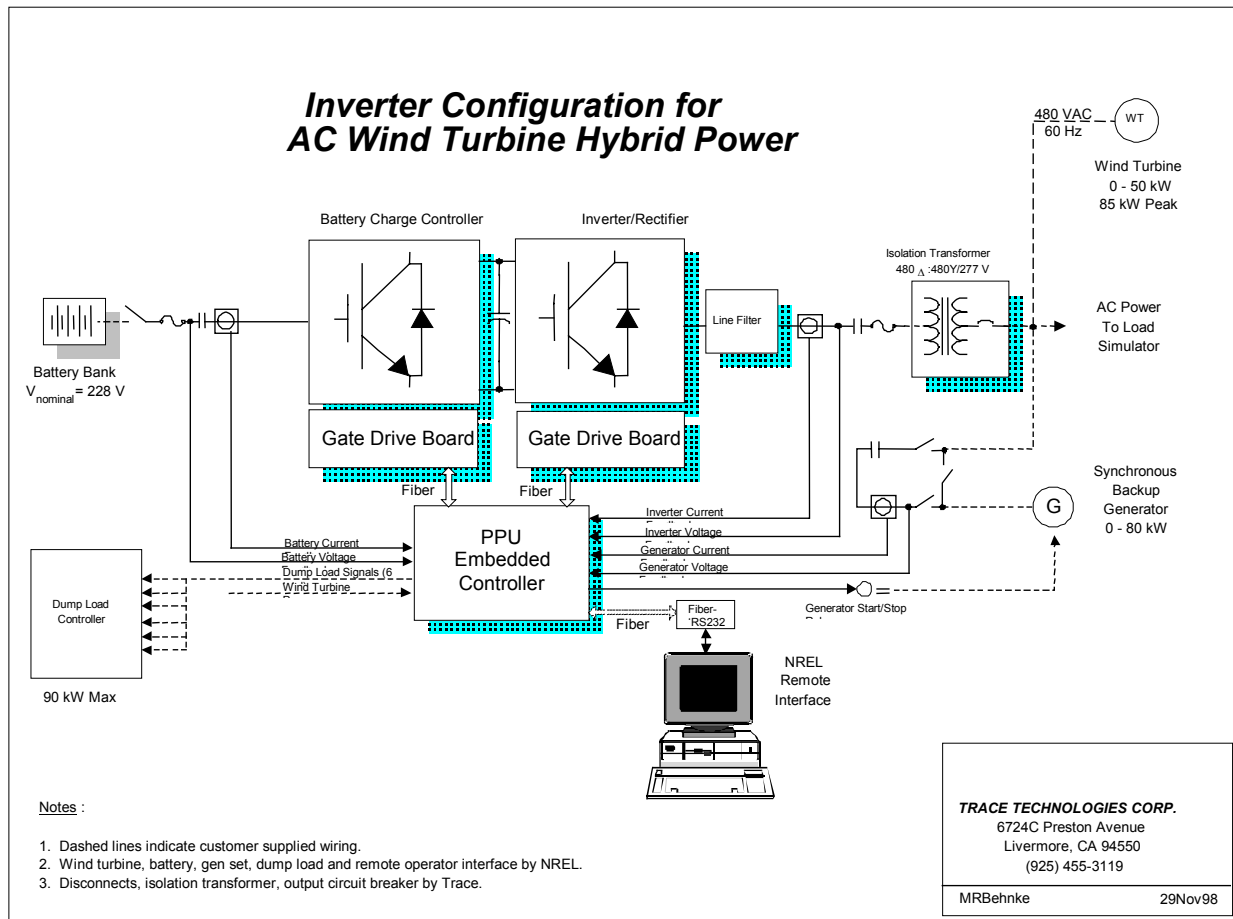


Figure 2. Wind-diesel hybrid system schematic.

8.2 Control Algorithms

Control algorithms that provided for robust operation under all possible conditions were written for the inverter controller. The basic inverter control algorithm is for operation of the inverter in a battery-charging configuration with an AC-connected wind turbine with 1) diesel connected or 2) diesel not connected. Additional control algorithms also include high-speed switching of a binary step dump load to control excess power flows from the wind turbine. The system was designed for a wind turbine with instantaneous power output (1-second average) from 0-85 kW, typical of an AOC 15/50. The inverter, which was connected to a 90-kW binary step dump load, supplied control signals (3-32 VDC) to control the zero crossing solid-state switches for the dump load elements.

The inverter control algorithms were designed for operation under the following conditions:

- No diesel gensets online — Wind turbine generator (WTG) power output from 0-85 kW with the WTG or batteries supplying load (depending on the “village” load and the WTG power output; i.e., net load) and the WTG charging the batteries when the

WTG power is greater than load. AC dump load is used for dissipation of excess power and to limit battery-charging current when the batteries are full.

- Diesel gensets online — The inverter operates in parallel with diesel gensets and the WTG; the diesel follows the load and the WTG power is used to charge the batteries or is dissipated by the dump load when the batteries are fully charged. During periods of no wind, the diesel may also charge the batteries.
- Control algorithms were designed to instantaneously shift power bi-directionally from the DC to AC bus.

The transition from diesel-on mode to diesel-off mode and vice versa is an important state transition that is controlled by the hybrid system controller and based on battery state of charge and net load (i.e., village load minus wind turbine output), as shown in Figure 3. A minimum load of about 10 kW is always kept on the diesel generator to prevent running the generator under a no-load condition. The maximum operating efficiency of the generator is at 80% or higher load. When the net load is low, the system transitions to a diesel-off state at a user-selected battery voltage so as to maximize wind turbine energy capture to the system. When the net load is high and the battery voltage is low, the system transitions to the diesel-on state so that the load can be met and the batteries charged. The specific parameters for the “matrix” shown in Figure 3 (see Appendix B) would vary depending on the type of battery bank.

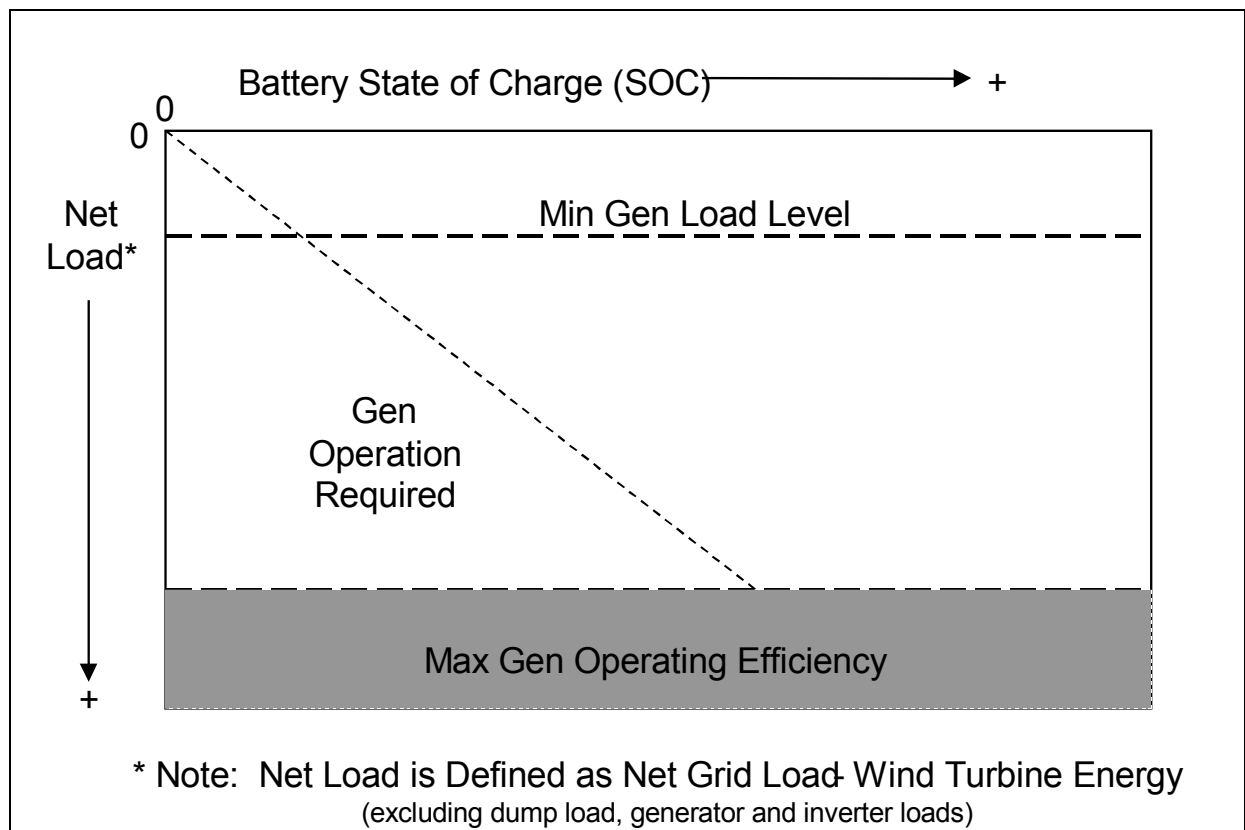


Figure 3. Dispatch matrix zones.

The top-level dispatch logic of the system can be found in Appendix B in the Matlab Simulink model. A key component of the dispatch logic is shown in Figure 4. The dispatch logic shows the control of the state transition from diesel-on mode to diesel-off mode or vice versa, depending on the battery SOC and the net load. The dispatch logic calls on the matrix tables (found in Appendix B and exemplified by the dispatch zones in Figure 3). Provisions were made for expanding the dispatch logic to include the rate of change of wind turbine power and net load.

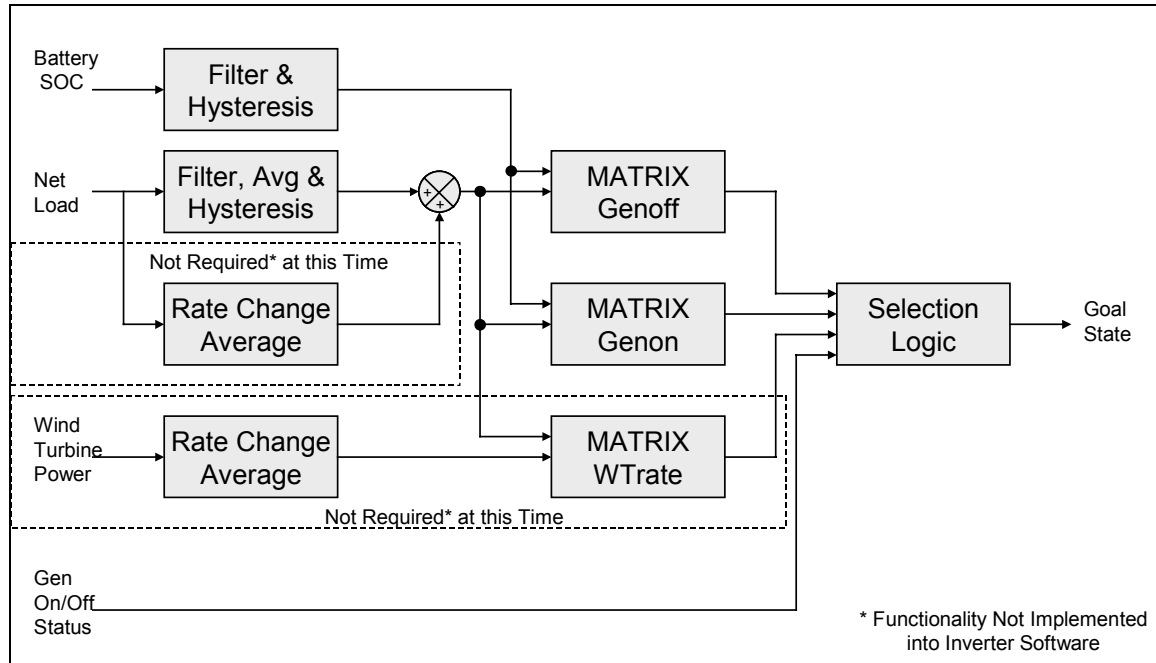


Figure 4. Top-level dispatch logic.

The charging algorithm is designed such that any energy produced in excess of the load is directed to the battery bank until the battery bank voltage reaches the dump-load-enable set point (Max_Bat_Hi). Once this set point is reached, the dump load is used to limit the charge current. The actual charge current during the finish charge stage is determined by the finish charge start and end voltage set points and the start and end charge current set points.

The converter control algorithms were developed based on the MATLAB Simulink model and the description above. This control logic was incorporated into a new revision of the HY-100 controller code by Xantrex engineers for testing at the National Wind Technology Center (NWTC). This code operated at the topmost level of the control code and did not run at the faster inner-loop control code that controlled parameters such as inverter frequency and voltage. The latest code revision for the hybrid controller code was NREL Tag revision 13.

9.0 Testing of the Modified Inverter

9.1 Hybrid Power Test Bed

Testing of the modified inverter was conducted at the NWTC's Hybrid Power Test Bed (HPTB). The HPTB is a multi-purpose test facility that combines a state-of-the-art Labview data

acquisition system with a switch panel that can easily switch in different “devices,” such as wind turbines, inverters, batteries, and load banks. A schematic of the HPTB test configuration for the Xantrex inverter testing is shown in Figure 5. All data sampling was conducted at 600 Hz, and the data averaging time is two seconds unless noted differently.

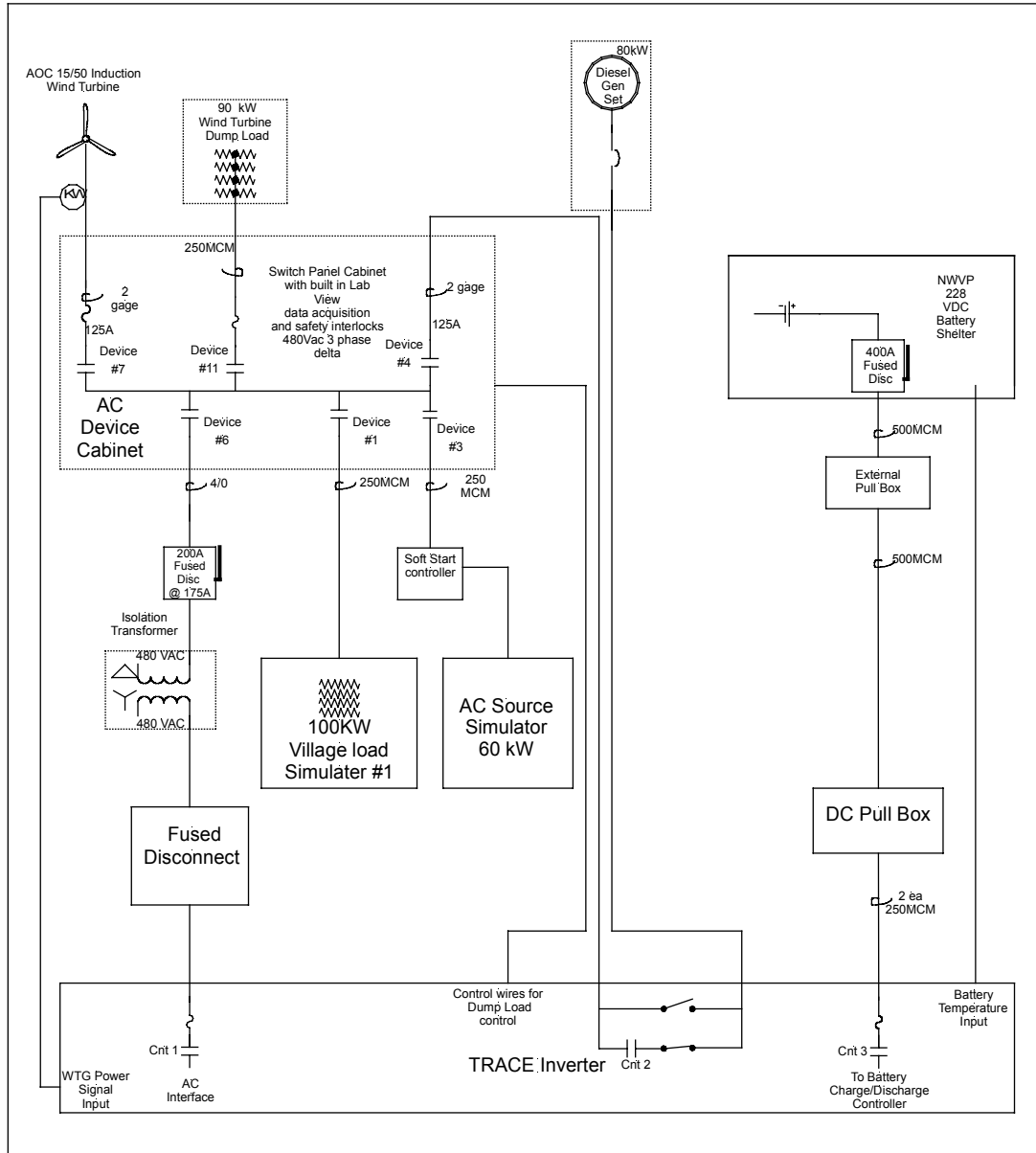


Figure 5. Hybrid Power Test Bed (HPTB) configuration.

9.2 Test Procedure

The testing goal for the Xantrex inverter was to conduct both dynamic and transient testing with the wind turbine or wind turbine simulator to verify that the inverter can handle expected conditions during operation. Due to unavailability of the AOC wind turbine, testing was conducted primarily with the AC source simulator. Testing with the AOC 15/50 was limited to wind turbine start-up tests and some steady-state tests.

The results of the test, along with the test procedures, may be found in Appendix C. A summary of the tests is contained in the rest of this section.

9.3 Functionality Checks

Before running the tests, functionality checks were conducted to verify proper inverter operation and state transition for steady- and quasi-steady-state operation. These checks verified that the system operated the way the hybrid controller intended it to operate, and any shortcomings were noted. Although many of these checks had been performed on previous software revisions for the hybrid controller, these checks were necessary to benchmark the latest revision of the software code. Before starting the test, all inverter settings were confirmed on the inverter and recorded. Details of the functionality tests may be found in Appendix C.

9.4 Test Results with AC Source Simulator

The AC source simulator is a variable-speed drive that is connected to a nominal 60-kW induction generator that has a soft start connected in series. It is controlled via the HPTB's Labview system. Control features include power setting and rate of power change.

The purpose of the testing with the AC source simulator was to verify that the inverter operated according to the control algorithms described in Section 8.2. This included verifying state transitions, with emphasis on transition from inverter state to charge and vice versa, as well as the battery charging algorithms. In addition, the system was tripped for special transient events such as the wind turbine "tripping" off-line at rated power. Because there is a limitation on the ramp rate for the power during contact closure, the AC source simulator could not "simulate" a hard start representative of an actual AC induction wind turbine.

The test setup for the AC Source Simulator can be seen in Figure 5. The test results are summarized in Appendix C, including time series plots from screen dumps for some of the tests.

9.5 Testing with the AOC 15/50 Wind Turbine

The purpose of this testing was to verify that the AOC 15/50 soft start was operational with the Xantrex inverter and that the inverter could bring the AOC 15/50 on to the grid without faulting the inverter or over-speeding the turbine. In addition, longer-term steady-state testing was conducted to verify that the system operated as designed.

Start-up testing was conducted to verify that the inverter could start the AOC 15/50 wind turbine. The inverter did start the AOC 15/50 several times; however, the test was not repeatable, and many times the AOC did not start successfully with the inverter but instead faulted on an over-speed condition. Changes were made to the AOC soft start to change the rate at which the soft

start would ramp the current and voltage, but an acceptable solution was not obtained. A solution that would allow the inverter to start the AOC reliably with the existing soft start is possible, but it would require further changes to the soft start and further testing, which is not possible under the scope of this project.

Once the AOC 15/50 turbine was online, the system ran without fault. Total run time with the AOC online was in excess of 80 hours, with much of the time in high winds (winds greater than 12 m/s), with good transitions between diesel-on mode and diesel-off mode.

10.0 Summary of Inverter Testing

Modifications were made to the TRACE HY-100 inverter to allow it to operate in a wind-diesel configuration with an induction wind turbine generator on the AC bus. The modifications included addition of a dump load to the system and modifications to the controller software to allow for battery charging and regulation of the system with the system operating with the wind turbine in both diesel-on and diesel-off modes (i.e., charge mode and inverter mode).

Testing was conducted to validate the modeling of the system and to verify operation with an actual wind turbine, including start-up with the AOC 15/50 wind turbine. The results of the testing were positive in that the inverter operated as designed with the wind turbine.

One shortcoming from the testing was that the inverter was not always able to start the AOC 15/50 wind turbine. Adjustments to the soft start of the AOC 15/50 wind turbine and further testing with the inverter would likely enable the inverter to start the AOC 15/50 wind turbine, but this work was not possible under the scope of this project.

A problem to be addressed in the future is the leading power factor for the inverter. When the inverter is used to power a mini-grid that has more than 15kVARs leading, it enters a state characterized by extreme harmonic distortion before faulting (approximately 10 seconds). This is a problem when certain loads have power factor correction capacitors that are always in the circuit, such as wind turbines with soft starts. This problem would need to be addressed through future work but does not appear to be a major impediment to the use of solid-state inverters with AC induction wind turbines in wind-diesel applications.

One drawback to the inverter is the standing losses. The standing losses, or “parasitic losses,” can be as high as 3 kW and should be included in any design for a wind-diesel system. Any attempts to use inverters of this topology in the future for wind-diesel systems should seek to reduce the standing losses of the inverter. One of the benefits that should be realized by a solid-state inverter as compared to a rotary converter for a wind-diesel system is higher efficiency, but the standing losses of the inverter prevent this.

Parallel operation of the inverter with a diesel generator was examined at the end of the project. This would allow the system to meet a load equal to the maximum power of the inverter plus the maximum power of the diesel, thereby increasing the capacity of the wind-diesel system. A description of this analysis is contained in Appendix D.

Appendix A: Xantrex HY-100 Inverter Description

The modified PPU will be a self-contained unit consisting of an inverter/rectifier bridge, a generator interface contactor, a diversion load controller, a battery charge controller, and their associated control electronics.

Inverter/Rectifier Bridge

Type: Three-phase, bi-directional, voltage-fed bridge converter

Switching Device: 1GBT, 1200V/600A rating

Switching Frequency: 10 kHz

DC Link Voltage: 420 VDC (regulated)

Nominal AC Output/Input Voltage: 208 VAC, three-phase, three-wire

Nominal AC Output Frequency: 60 Hz

Continuous kVa @ 208 VAC

Surge Capability: 150% of continuous rating for 10 seconds

Load Power Factor: 0 lagging to 0 leading

Hardware-Based Protection

Voltage Transient: MOV-type surge arrester, 650V MCOV, 20 kA surge current (8x20us) capability, ANSI/IEEE C62.41 Category C

Short Circuit: Current-limiting semiconductor fuses, 300 A continuous, 200kA interrupting capacity

Generator Interface

Contactor Rating: 100 kVA @ 208 VAC (300 A continuous)

Start/Stop Relay: Normally open contact rated 12 amps @ 480 volts

Disconnects: 600 VAC, 400 A, three-pole load-break disconnect switches for generator input and output located in enclosure mounted on side of PPU enclosure

Bypass: 600 VAC, 400 A, three-pole load-break disconnect switch for bypass of PPU in common enclosure with generator disconnects

Battery Charge Controller

Type: Bi-directional, current regulated, DC-DC buck and boost converter

Switching Device: IGBT, 1200V/600A rating

Switching Frequency: 10 kHz

Nominal Battery Voltage: 228 VDC

Maximum Equalizing Voltage: Field settable to 300 VDC

Low Voltage Cutoff: 200 VDC (1.75 VPC)

Battery Manual Disconnect Switch: 440 VDC, 600 A, three pole, load break disconnect switch

Operator Interface

LCD/Keypad: Piezoelectric keypad and two-line LCD display located on door of enclosure

Enable/Disable Switch: Keypad enable/disable switch located on door of enclosure

E-Stop: Maintained-position, mushroom head emergency stop button located on door of enclosure

Control States

The PPU shall be a state-controlled machine with clearly defined valid states and state transitions for each of the PPU components. Except during state transitions, the PPU shall always reside in one of five states, as described below.

Inverter State

- Inverter/rectifier bridge regulates AC line voltage
- Generator off-line
- Inverter controls diversion load to limit battery charge current
- Battery charge controller regulates DC bus

Generator Support State

- Generator online, regulating AC voltage
- Inverter/rectifier bridge regulates DC bus
- Battery charge controller regulates generator load current (including support of generator in AC-current regulation mode if load exceeds generator rating. Generator support refers to current flow from the PPU to the grid should the load power exceed the generator power rating.)
- Inverter controls diversion load to limit battery charge current

Equalize State

- Generator online
- Inverter/rectifier bridge regulates DC bus
- Equalize can be set for Manual or Automatic Mode
- Automatic Equalize will occur at a field-settable interval of 1 to 100 days

Generator Only State

- Generator online
- Inverter/rectifier bridge, battery charge controller and diversion load control disabled

Blackout State

- Generator and wind turbine offline
- Inverter/rectifier bridge, battery charge controller and diversion load control disabled

Inverter/Rectifier Bridge Control

Inverter State Control Method: Current-regulated pulse-width-modulation (PWM), with AC line voltage outer control loop; voltage references generated by embedded controller

Generator Support and Equalize State Control Method: Current-regulated, sinusoidal PWM, with DC bus voltage outer control loop; current references derived from generator voltages

Battery Charge Controller Control

Inverter State Control Method: Current-regulated PWM, with DC bus voltage outer control loop

Generator Support Control Method: Current-regulated PWM, with battery voltage and generator current outer control loops; all charge algorithm set points field settable

Equalize State Control Method: Current-regulated PWM, with battery voltage outer control loop; all equalize algorithm set points field settable

Generator Start Voltage: Field settable from 0 to 350 volts, with field-settable current and temperature compensation factors

Charge Voltage: Field settable from 0 to 350 volts, with field-settable current and temperature compensation factors

Low Voltage Discharge Cutoff: Field-settable from 0 to 350 with field-settable current compensation factor

Equalization Voltage: Field-settable from 0 to 350 volts with field-settable current compensation factor

Equalization Timer: Field-settable from 0 to 168 hours

Equalization Interval: Field-settable from 1 to 100 days

Generator Interface Control

Warm-Up Time Delay: Field-settable from 0 to 20 minutes

Cool-Down Time Delay: Field-settable from 0 to 20 minutes

Instrumentation

Instrumented Parameters: The following parameters shall be available through the operator interface LCD and transmitted to the optional DAS. Instrument error shall not exceed 2.5% of full-scale values, unless otherwise noted.

Inverter Voltage	Generator Voltage
Inverter Current	Generator Current
Inverter Real Power	Generator Frequency
Inverter Reactive Power	Generator Real Power
Inverter Frequency	Generator Reactive Power
Battery Voltage	Alarm Codes
Battery Current	Heat Sink Temperature
Battery Power	Operating State

Communication Medium: Fiber-optic pair; fiber ports provided on PPU embedded controller

Communication Medium: Fiber-optic pair; fiber ports provided on PPU embedded controller

Communication Protocol: Supplied by subcontractor

Self-Protection, Fault Detection, and Alarms

Embedded controller algorithms will include the following fault detectors. All faults are latching and result in an automatic transition to a fault state. If the generator is operating at the time of the fault, the generator start-stop contact and generator contactor will remain closed. If the generator is not operating, the start/stop contact and generator contactor will close. Upon clearance of the fault from either the operator interface or the optional DAS, the PPU will transition to either the Generator Only or Blackout state, depending on the operating state of the generator.

Fault	User Settable?	Setpoint Range
Serial communication timeout	No	N/A
Interrupt timeout	No	N/A
Matrix control failure	No	N/A
State machine failure	No	N/A
Bus precharge fault	No	N/A
Bus regulation fault	No	N/A
DC bus overvoltage	No	N/A
DC bus undervoltage	No	N/A
Gate drive fault	No	N/A
Matrix overtemperature	No	N/A
Magnetics overtemperature	No	N/A
DC ground fault	Yes	0 to 100 A
Emergency stop	No	N/A
Key switch	No	N/A
Door interlock	No	N/A
Battery overvoltage	No	N/A
Battery overcurrent	No	N/A
Battery low voltage disconnect	Yes	0 to 350 V

Inverter overvoltage	Yes	208 to 250 V; 0 to 10 sec
Inverter undervoltage	Yes	166 to 208 V; 0 to 10 sec
Inverter overfrequency	Yes	60 to 65 Hz; 0 to 10 sec
Inverter underfrequency	Yes	55 to 60 Hz; 0 to 10 sec
Inverter overcurrent	No	N/A
Generator overvoltage	Yes	Same as inverter
Generator undervoltage	Yes	Same as inverter
Generator overfrequency	Yes	Same as inverter
Generator underfrequency	Yes	Same as inverter

Performance Specifications

EMI/RFI Emissions: Not to exceed FCC Part 15 Rules for Class A device

Efficiency (exclusive of transformer losses): > 94%

Voltage Regulations: $\pm 5\%$ of nominal, phase-to-phase

Frequency Regulation: ± 0.5 Hz of nominal

Voltage Distortion: Less than 5% THD under linear load

Battery Voltage Ripple: 5 V maximum (2% of nominal battery voltage)

Appendix B: MATLAB Dynamic and Transient Wind-Diesel Models

NREL Dispatch Dynamic Model Document

1.0 Scope

This document provides toplevel instructions for running the MATLAB NREL Modified Inverter Dynamic model. Also included are descriptions of the various functions within the model along with their flow diagrams.

This model is based on an energy balance between a wind turbine, inverter/battery, generator, grid load and dump load elements. Logic for transitioning between states is computed by the MATRIX logic function. The MATRIX logic uses filtered/averaged values for battery state-of-charge (SOC) and net load demand to determine which operating state should be requested. The battery's SOC is assumed to be related to the battery's voltage and the grid's net load demand is defined as grid load minus wind turbine output in kW.

The time step for this model is based on 1.0 SIMULINK model step = 1.0 second simulation time. The minimal inputs include a time vector (sec), grid load vector (kW) and a wind speed (mps) vector. The outputs are located within in the toplevel diagram of the model and duplicated within the "Control Panel" for ease of use. The output values include; generator on cycles, generator fuel usage, lost energy (dump load) and generator run time.

2.0 Requirements

The NREL Dispatch model was developed using Math Works MATLAB SIMULINK program. Therefore to run the model you will need to have MATLAB software, with the SIMULINK option installed on your computer. Please note this model was developed on an IBM compatible PC.

The initial model development used MATLAB Version 9. Several compatibility issues, with Windows '98, were encountered early on and therefore the MATLAB program was upgraded to Version 11.0 for all further developmental efforts. It is recommended that Version 11.0, or later, be used to run this model.

NOTE: This document was written assuming the operator has a familiarity with the program MATLAB/SIMULINK, although I have tried to cover each step in enough detail so you do not need to be an expert.

3.0 Operating Procedures

The procedure for running the model involves five steps A) opening the model in MATLAB/SIMULINK, B) set-up the input vectors, C) modify model settings (as required), D) run the model and finally E) review the data. Each step is discussed in more detail below. [Note: any input, to be typed in from the keyboard, is identified by enclosing the text within \diamond brackets. The greater than/less than brackets are not part of the input.]

Step A) Open the NREL_dyn model in MATLAB

- 1) Open the MATLAB program as any Windows based program. This will open a MATLAB workspace titled 'MATLAB Command Window'.
- 2) At this point you may want to load any previously saved workspace variables using the <load 'filename'> command. See 'Step B' below for more details.
- 3) Now type <simulink> and hit enter. This will open the SIMULINK portion of the program.
- 4) Under File on the Library:SIMULINK window menubar select 'Open'. Locate the appropriate directory and find the file named nrel5dy0.mdl. Double click on the file.
- 5) You should now have the MATLAB workspace, the Library:SIMULINK toolbar, the model nrel5dy0 and an Untitled SIMULINK Window open. Note, you can close the Untitled SIMULINK Window since it will not be used.

Step B) Set-up the Input Vectors

You will need to provide a time, grid load and wind profile "vector" to the SIMULINK model. To make the vector data available to the model, it must exist in the MATLAB workspace environment. The model's input variables include the following:

Variable Name	Description	Units
T	A column vector for time	seconds
U	A column vector for grid load	kW
W	A column vector for wind speed	mps

Four additional variables must exist in the MATLAB workspace environment, they are;

MXEVON1	A 10 X 10 matrix for the gen on State conditions, function of Net load and battery SOC (evaluation settings)
MXEVOFF1	A 10 X 10 matrix for the gen off State conditions, function of Net load and battery SOC (evaluation settings)
MXBLON1	A 10 X 10 matrix for the gen on State conditions, function of Net load and battery SOC (baseline settings)
MXBLOFF1	A 10 X 10 matrix for the gen off State conditions, function of Net load and battery SOC (baseline settings)

The four matrix variables, with default settings, are included in the dynenv.mat file. This file should be copied into the same directory where the SIMULINK model is located. Prior to opening the SIMULINK model, type the following; <load 'dynenv.mat'> to load the default environmental variables. Note: this file also contains several developmental cases which can be used for diagnostic purposes.

The time step is based on 1.0 = 1.0 second which matches the dynamic model's imbedded time constants. Also note that it takes the first ten minutes of simulation time to completely "initialize" the various simulation filters. This should be taken into account when defining your input vectors. To load the time, grid load and wind speed vectors perform the following steps.

- 1) Click on the MATLAB workspace, to make it the active window.
- 2) Now you can enter the data manually or load it from a previous secession, using the save and load commands. To retrieve data saved from a previous secession, type <load 'filename'>. To verify the vectors are available you can type <who> in the MATLAB workspace and the available variables will be listed.
- 3) To load the data manually, type the following for the T, time, vector; < T = [0:step:endtime]'; >. Where step is the value of the time step desired and endtime is the end time value. Note: the ' character will transpose the vector from horizontal to a vertical vector. Also the ; will suppress the values of the vector from being echoed to the workspace.
- 4) To manually load the U, grid load, vector type the following; < U = [u1 u2 u3 ...]'; >. Where u1, u2, u3 ... are grid load values for the time steps defined in 'Step C'. Remember the first time value is 0.0.
- 5) To manually load the W, wind speed, vector type the following; < W = [w1 w2 w3 ...]'; >. Where w1, w2, w3 ... are wind speed values for the time steps defined in 'Step C'. Remember the first time value is 0.0.

Step C) Modify Model Settings

- 1) To modify any of the model parameters first click on the NREL_dyn model window to make it the active window.
- 2) Now click on the particular item you wish to change. A window will open with instructions on which changes are allowed.
- 3) Below are a few of the parameters one might want to modify;

<u>Item to be Modified</u>	<u>Location</u>
Number of wind turbines	Control Panel
MATRIX config. (baseline or eval)	Control Panel
Wind Speed pre-processing	Wind Plant Simulation

State Matrix variables (for Gen On)	MATRIX Logic/ Gennon MATRIX
State Matrix variables (for Gen Off)	MATRIX Logic/ Genoff MATRIX
Gen fuel Usage	Gen Fuel Usage/ Load to Fuel Table
Inverter Charge Rate (high)	Control Panel
Inverter Charge Rate (low)	Control Panel
Dump Load Rate Limit	Inverter Model/ Rate Limiter1
Min Gen Load Level	Control Panel
Min Inv. Load Level (when battery fully charged)	Control Panel
Min Dump Load Level	Control Panel
Dump Load Rise Rate	Inverter Model/ Dump Load Logic/ Dump Load Controller/ Inc Rate
Dump Load Fall Rate	Inverter Model/ Dump Load Logic/ Dump Load Controller/ Dec Rate
Initial Battery Capacity	Battery Model/ Integrator initial value (Set Inverter Model/1 to 10 Hyst Bat/Hyster 5 min/ Unit Delay Initial values to prevent start-up conflicts)

Step D) Run the Model

- 1) Once the input vectors are defined and any modification made to the model, you are now ready to run the model. This is accomplished by clicking the 'Simulation' button on the Menu bar of the NREL_dyn model window and clicking 'start'. Note: you should verify the simulation start and end times are consistent with the time input vector. These values can be found by selecting Parameter under the Simulation menubar item.
- 2) Depending on the size of the input vectors and the speed of your computer the run time can take several minutes to hours. Typical runs have taken up to 2 hours to run a 24 hour simulation (based on a 350 mHz PII processor).

Step E) Review the Data

- 1) After running the model you can review the data collected by opening the various 'scopes' within the model.
- 2) Several key values are displayed on the toplevel model window. These include; Lost Energy, Generator Run Time, Generator Fuel Usage and Generator On Cycles.
- 3) The four key output values, identified above, are also located in the Control Panel sub-function, for the users convenience. Also included are seven control variables that can be manually set from the Control Panel (identified in 'Step C').
- 4) If you want data transferred to the MATLAB workspace for further analysis, add an output port to the appropriate location and then connect it to the desired variable data line. The output port (To Workspace block) can be obtained from the SIMULINK Library Browser under the Simulink/Sinks window. Click and hold on the icon and drag it to the appropriate model window. Once on the model window release. You can now move the output port to a location close to the signal line of the variable you are looking for. With the cursor over the signal line depress the 'Ctrl' key and the left mouse button and hold. Now move the cursor to the connector on the output port. Once at the proper location release. You should now have a data line connected to the output port. Now set the properties of the block by double clicking on the icon.

4.0 Function Descriptions

There are nine main sub-functions that make-up the model, each containing additional sub-function for ease of documenting. Below is a listing of each one along with a short description. Under most conditions there will be no need to access these functions but an understanding of them will assist in the proper usage of the model and its limitations.

1) Wind Plant Simulation

This sub-function includes four wind turbine models for calculating the wind turbine energy delivered to the grid. The number of wind turbines used by the simulation can be controlled by the "Number of Turbines" variable in the Control Panel. An off-set value and transfer function are included to modify the wind speed input, to the turbines, to more accurately represent the power produced by a "windplant". These values can be modified as required. This function also includes the four sub-functions titled "Wind Turbine # Model".

2) Wind Turbine # Model

This sub-function models a simple constant speed induction generator type wind turbine. Stall/Pitch control is used to limit max power output. The wind turbine aero dynamics are modeled by a simple first order lag with a 0.5 sec time constant. The stall/pitch system is modeled using an integrator and first order lag of a 0.1 sec time constant. This in turn modifies a "Kp" value which emulates the changing energy capture of the turbine. The loop is closed on a reference max power setting which is set at 62 kW.

Wind Turbine Model Assumptions:

- 1) Output power is the product of the modified input wind speed and Kp value. Kp is obtained from the "NREL Kp Look-Up Table1" which uses a "pitch angle" to set the wind turbine's energy capture capability.
- 2) The output power below rated is assumed to be linear with wind speed, therefore a fixed Kp value at full power "pitch" is used. If the output power needs to be modified the "WS Look-Up Table2" can be used to modify the input wind speed to achieve the appropriate output power.
- 3) Pitch control is assumed to regulate max power. The dynamic response of the pitch system is defined by the Pitch Dyn (transfer function) block. The pitch integrator is limited to the min and max pitch values. The dynamics were based on the following:
Step 0 to 20 mps results in a peak power of ~ 85 kW and a settling time of ~ 4 sec. Rated power set at 62 kW.

3) Matrix Logic

This sub-function includes the logic to determine the desired control "State" the inverter should operate in. The MATRIX tables contain the desired operating states as a function of Net Load and Battery State of Charge (SOC). Note: these signals are filtered/averaged values, not the "raw" input signals. There are two MATRIX tables, for each configuration, one for when the generator is presently off (gennoff) and the other for when the generator is presently on-line (gennon). The logic selects from the appropriate table depending on the existing state of the generator. The operator can also select from two different MATRIX configurations. One is labeled "Baseline" and can be used for comparisons to other MATRIX configurations. It presently contains values to emulate the original inverter operation. The other table, labeled "Eval" should be used for new logic development. The values of these look-up tables can be modified as required. The values are included in a 10 X 10 matrix located in the MATLAB work environment. The matrixes are named;

MXBLON	Baseline Gen On
MXBLOFF	Baseline Gen Off
MXEVON	Evaluation Gen ON
MXEVOFF	Evaluation Gen Off

This function also includes the sub-functions Gen-on Trans, Gen-off Trans and HCU States which control the states transitions. The Gen-on and Gen-off blocks include logic for transitioning between inverter and generator operation. They both include a hold state and a ramp state (or transition state). The hold state emulates the condition where the inverter is preparing to transition and the ramp state emulates the condition where the inverter is ramping the load to or from the generator. For generator on transitions the hold state is 2 and the ramp state is 1. The actual transfer occurs when the inverter load reaches a set value defined by the Inv_Low signal. This signal is calculated in the Ramp Inv Off sub-function.

For the generator off transition the hold state is 5 and the ramp state is 0. The actual transfer occurs when the generator load reaches a set value defined

by the Gen_Low signal. This signal is calculated in the Ramp Inv On sub-function.

The hold and ramp times are settable. Refer to the appropriate block diagram for directions for setting these variables.

The HCU sub-function generates a Mux State signal containing the various state conditions. These include the transient_state, gen state, and current HCU state.

4) Battery Model

This sub-function models the battery storage hardware. The gain1 variable sets the battery charge efficiency. The discharge efficiency is assumed to be 100%. The battery voltage is output as a measure of the battery capacity. The table "V Look-Up Table" converts battery capacity, in Amp-Hrs to Volts per cell. "# of Batteries" is the number of battery cells to obtain the total battery output voltage.

5) Generator Model

This sub-function models the generator hardware. The Integrator, Gain and "Gen Dynamics" functions model's the generator power production dynamics. The Gain1 variable is used to quickly return the integrator to zero output to prevent integrator wind-up when the generator is turned off.

6) Dump Load Model

This sub-function models the dump load hardware. The "D to A" term is used to convert the six bit digital signal to an actual dump load level. The "Dump Load Dyn" function models the dump load dynamics.

7) Inverter Model

This sub-function models the Inverter hardware and logic. First, the operating state, as defined by the MATRIX logic, is decoded and the proper inverter action is taken.

<u>State</u>	<u>Description</u>
State 0	Transition from Generator on to Inverter on
State 1	Transition from Inverter on to Generator on
State 2	Generator off and inverter supplying net load (Voltage source)
State 3	Generator on and inverter charging battery, at a high constant rate
State 4	Generator on and inverter charging battery, at a low constant rate
State 5	Generator on and inverter off

This function also includes the inverter control dynamics (Inv Ramp On/Off, Inverter Dyn., and Inv. Gain sub-functions), averaging and "digitizing" of the net load (1 to 10 Hyst Load function) and battery filtering and SOC (bat filter and 1 to 10 Hyst Bat functions) output values, and the dump load binary output signal (Dump Load Logic, A to D and Change to Integer functions).

8) Dump Load Logic

This sub-function models the dump load logic. It generates the dump load control signals (dump load hold signal, generator on signal, transition to generator on signal, and battery SOC at max when the inverter is providing the net load) for determining if the dump load should be turned on, off or hold last value. This function also includes the "Dump Load Controller" sub-function.

9) Dump Load Controller

This sub-function models the dump load controller logic. If the conditions are right, 1) generator output level is below its min level or 2) the battery max charge is exceeded and the grid has excess energy, with the inverter controlling the grid, then the dump load is activated. At this time the dump load level is set by a simple proportional plus integral controller which increases the dump load quickly to resolve the above conditions and then reduces the load demand, at a slightly slower rate, as the condition returns to "normal". The proportional error term is single sided to increase the dump load during extremely fast transients. The integrator rates are set by the variables "DUMP_INC_GAIN" and "DUMP_DECR_GAIN". The "Min gen Level" and "Min Inv level" values set the lower operating power level for the generator and inverter respectively. This function also includes the "Integ/Limt" sub-function which actually calculates the dump load commanded value.

10) 1 to 10 Hyst Load

This sub-function models the logic to filter and then convert, to an integer value, the input signal "calculated net load" (negative value of the sum of inverter load, generator load, and dump load demand). The input signal first passes through a filter and averaging function contained in the "Digital Lag/Avg" sub-function. The filter is a first order lag filter (time constant of ~ 125 sec). The signal is then passed through a running average filter using five values updated, in series, every 60 seconds. This results in an overall effect similar to a first order lag filter with a ~ 300 sec time constant but the settling time is much faster, ~ 800 sec.

Next the signal is scaled and converted to an integer value by the sub-function "Hyster". The conversion assumes no rounding-up and using a +0.5 hysteresis on the decrease side. The output value is updated every 200 seconds. The output signal is also limited to a range between 0 and 9. This range is the present limits of the input values to the MATRIX tables. The output signal is labeled "Net load Int".

NOTE: The input signal defined above "calculated net load" was assumed to most accurately reflect the value for "Net Load" as defined as grid load minus wind turbine output.

11) Bat Filter

This sub-function performs a first order filter of the battery voltage signal, provided by the inverter controller. The time constant is presently set for ~124 sec.

12) 1 to 10 Hyst Bat

This sub-function models the logic to convert, to an integer, the input signal "Bat Volt Filt". The input signal is first converted from a voltage to a value representing the battery "State of Charge" (SOC). This is performed by the "V to Units Look-up Table" sub-function. The "Hyster" sub-function is the same as the hysteresis function previously discussed, except it uses a 600 sec

update rate. Also included is logic to detect a low battery condition and set the output signal to a low value, in real time. This additional logic is required to override the imbedded time delay of the "Hyster" sub-function. The output signal is labeled "Bat Volt Int".

NOTE: Filtering on this signal was moved outside this function because of the need for additional filtering on the battery voltage signal going to the dump load logic.

13) Inv Ramp On/Off

This sub-function models the inverter logic for transitioning the load to/from the inverter during generator on/off transients. The load demands during transfer conditions are calculated in the "Ramp Inv Off" and "Ramp Inv On" sub-functions. They use the various current state values and ramp times (Ramp_Off and Ramp_On variables) to determine the timing and rates to transfer the loads. They also calculate the signals (Inv_Low and Gen_Low) used for switching between generator and inverter operation during the transition.

Part 5 SIMULINK Diagrams of Dispatch dynamic Model

Model Name: "nrel5dy0.mdl" Version 5.0 Rev 0

NREL Modified Inverter Model Revision Notes

Version 1.0 Baseline

- Rev 1: Changed 0 to 6 Hyst Logic, in Inverter Model, to simulate C code implementation
- Rev 2: Integ/Limit mod for C code implementation
- Rev 2: Changed Inc rate from 2.0 to 0.02 & Dec rate from 0.3 to 0.003
- Rev 2: Added step function to force start-up in Inverter mode, Required due to unit step delays in hyst function
- Rev 2: Changed MATRIX Genon(1,3) from 3 to 2
- Rev 3: Changed First order lag (4 Step Lag) function to discrete implementation (Digital Lag)
- Rev 3: Updated wind turbine model for TSR input to Kp Table
- Rev 3: Added offset to windspeed inputs to turbines #2,3 and 4
- Rev 3: Modified turbine logic to divide power delta by speed to get torque into integrator
- Rev 3: Added Ref Speed to properly calculate output power
- Rev 3: Add real time low battery condition logic

Version 2.0 Update to NREL H/W Configuration, Time Step set to 1.0 = 1.0 sec

- Ver 2.0 Mod grid Dynamics for NREL H/W
- Ver 2.0 Change values for NREL H/W (Battery Model)
- Ver 2.0 Modify for NREL H/W Config (battery off-set voltage)
- Ver 2.01 to 6 Hyst Bat: Modify for NREL H/W (Battery Voltage to Storage)
- Ver 2.0 Hyster: Update Unit Delay and Saturation Limits
 - Rev1: Added Rate Limiter to Relay to stabilize dump load while gen operating
 - Rev1: Removed Rate Limiter from Gen Model to Investigate stability issue
 - Rev 1: Added H/W delays to Dump Load Variables
 - Rev1: Changed Gain from 0.02 to 0.008 to minimize potential aliasing in Averager

Version 4.0 Conversion to MATLAB Release 11 and Mods for S/W compatability

- Ver 4.0 Changed 'Inv err signal' to Net Load and Dump Load Logic to Inverter 'load' value
- Ver 4.0 Changed 'Inv err signal' to Inverter 'load' value & required Dump Load controller changes
- Ver 4.0 Added min Inv Load for dump load Controller
 - Rev 1.0 Change Charge to Discharge (high)
 - Rev 1.0 Changed max dump load to 90 kW
 - Rev 1.0 Change Saturation Limits to 0 to 9
 - Rev 1.0 Change # Batteries to 114 & V to Units Table values
 - Rev 1.0 Changed Max Bat Level to 250 on & 243 Off
 - Rev 1.0 Changed MATRIX row range to 0 to 9 and use new MATRIX tables
 - Rev 1.0 Added filter to battery signal
 - Rev 1.0 Removed dump load rate filter (redundant)
 - Rev 2.0 Added gen transition on logic to dump load
 - Rev 2.0 Changed start-up state to 2 (State 1 now represents gen transitioning on)
- Rev3.0: Removed initial lag of Sum2 digital filter, not required.
- Rev3.0: Modified Dump Load Integ/Limit function (added proportional gain term and mod rate limits)
- Rev 3.0 Added minimum dump load value
- Rev 4.0 Changed Battery Hyster input delay to 600 sec ZOH & output delay to 1 sec
- Rev 4.0 Changed Load Hyster input delay to 200 sec ZOH & output delay to 1 sec
- Rev 5.0 Added HCU_SYNC_TO_INV lock-out on gen_dump_on signal
- Rev 6.0 Updated Inverter transition on/off logic
- Rev 6.0 Modified State transition logic for gen on/off
- Rev 6.0 Modified start-up state to 0 to minimize transients

Version 4.0 Conversion to MATLAB Release 11 and Mods for S/W compatability

- Rev 7.0 Increase Grid Dynamics to 0.01 sec time constant
- Rev 7.0 Increase Gen Dynamics (Based on NREL best guess on 9/30/99)
- Rev 7.0 Modify Inverter Dynamics (faster response best guess 10/1/99)
- Rev 7.0 Changed start-up state to 2
- Rev 7.0 Changed DUMP_RATE_MIN to -20
- Rev 7.0 Changed DUMP_DECR_GAIN to 0.3
- Rev 7.0 Added hold function to Integ/limit1 function
- Rev 7.0 Added Dump Hold logic
- Rev 7.0 Removed HCU_SYNC_TO_INV state lock-out on gen_dump_on
- Rev 7.0 Calculated GEN_TRAN signal for dump logic
- Rev 7.0 Added GEN_TRAN signal for gen_tran signal
- Rev 7.0 Change sign of input (gen load) signal
- Rev 7.0 Changed DUMP_PERR_GAIN to 3.0 due to faster gen dynamics

- Rev 8.0 Modified Inverter On/Off switch to account for load transfer to/from Gen
- Rev 8.0 Changed gen_dump_on signal to account for transition states
- Rev 8.0 Added Ramp_Off calc to automate trans. load
- Rev 8.0 Added Ramp_On calc to automate trans. load
- Rev 8.0 Added Ramp_Off signal to set load transfer rate
- Rev 8.0 Added Ramp_On signal to set load transfer rate
- Rev 8.0 Calc Gen_Low signal to determine min gen load during tranfer of load
- Rev 8.0 Added low gen load transfer for load transition
- Rev 8.0 Added delay to Gen_Low signal to address algebraic loop

- Rev 9.0 Added transient_state calc/output INV_TO_SHUTDOWN
- Rev 9.0 Added Transition state calc/output SHUTDOWN_TO_INVERTER
- Rev 9.0 Add state mux signal
- Rev 9.0 Added Demux for State Signal Scope
- Rev 9.0 Added Demux to input state signal
- Rev 9.0 Changed to Gen On Line state for gen On/Off signal
- Rev 9.0 Revised gen_tran signal to use transition_state
- Rev 9.0 Revised gen_dump_on signal to use gen_state on
- Rev 9.0 Changed bat_level_high to use only HCU_INV condition
- Rev 9.0 Added Demux signal to State input

Version 5.0 NREL Deliverable Version

Ver 5.0 Updated Dump_Hold logic (revoved HCU_SYNC_TO_SHUTDOWN)

Ver 5.0 Mod gen_dump_on to include GEN_RAMP state (no real change required)

Ver 5.0 Updated ramp time and added Inv_Low transition

Ver 5.0 Moved location of Gen_Low transition logic

Ver 5.0 Added Inv_Low Calc and mod ramp off logic

Ver 5.0 Modified calc of Off ramp timers constant = [Rate] and constant3 = [pt]

Ver 5.0 Modified On Rate time variable inputs [Rate] & [pt] for simplify

Ver 5.0 Added ZOH to accuratly represent S/W Implementation

Ver 5.0 Changed Net load Unit Delay to 200 sec

Ver 5.0 Changed battery Hyst Unit Delay to 600 sec

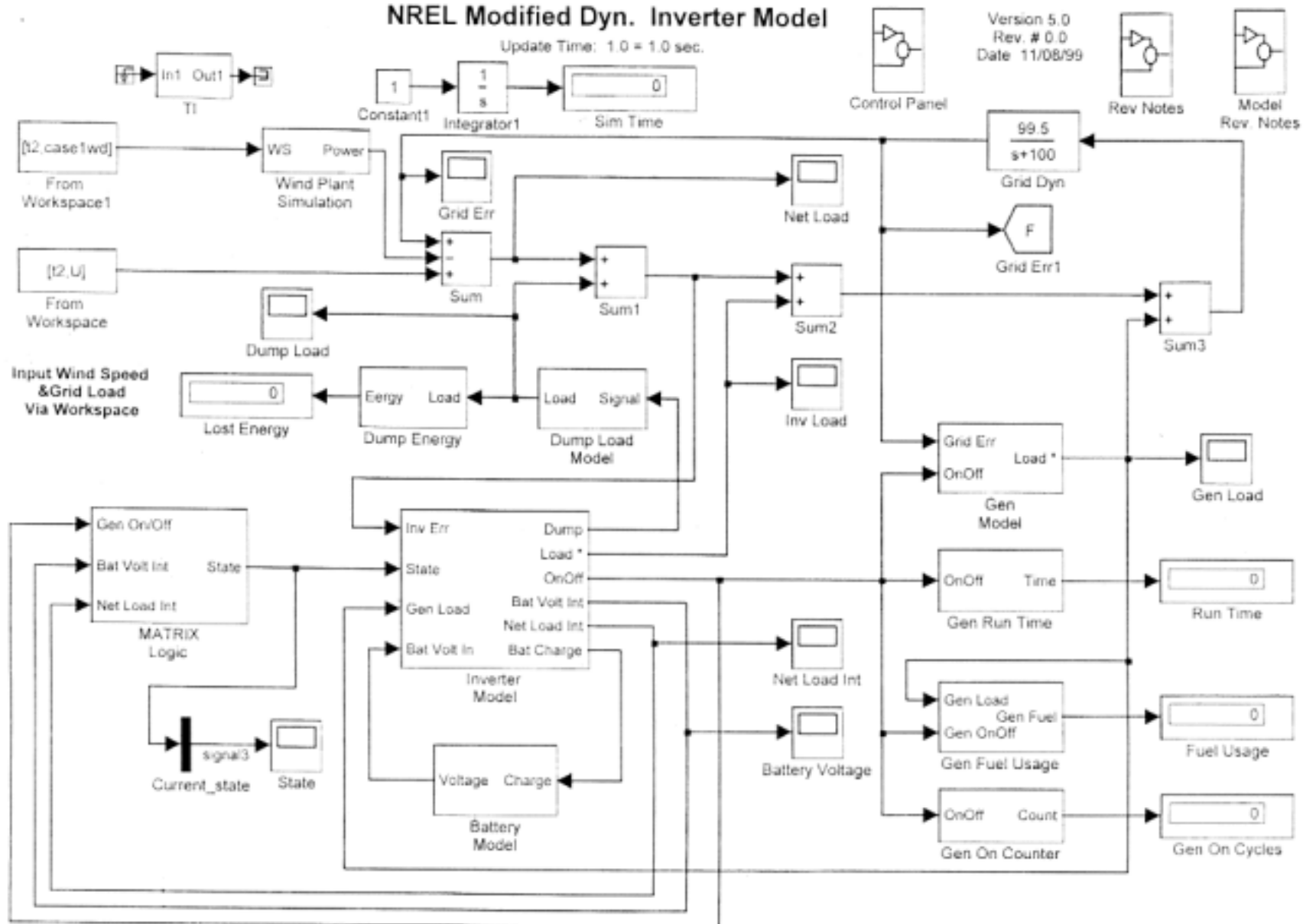
Ver 5.0 Incorporated wind turbine sim into model

Ver 5.0 Modified Integrator Rate limits and added ZOH (better simulate actual code)

NREL Modified Dyn. Inverter Model

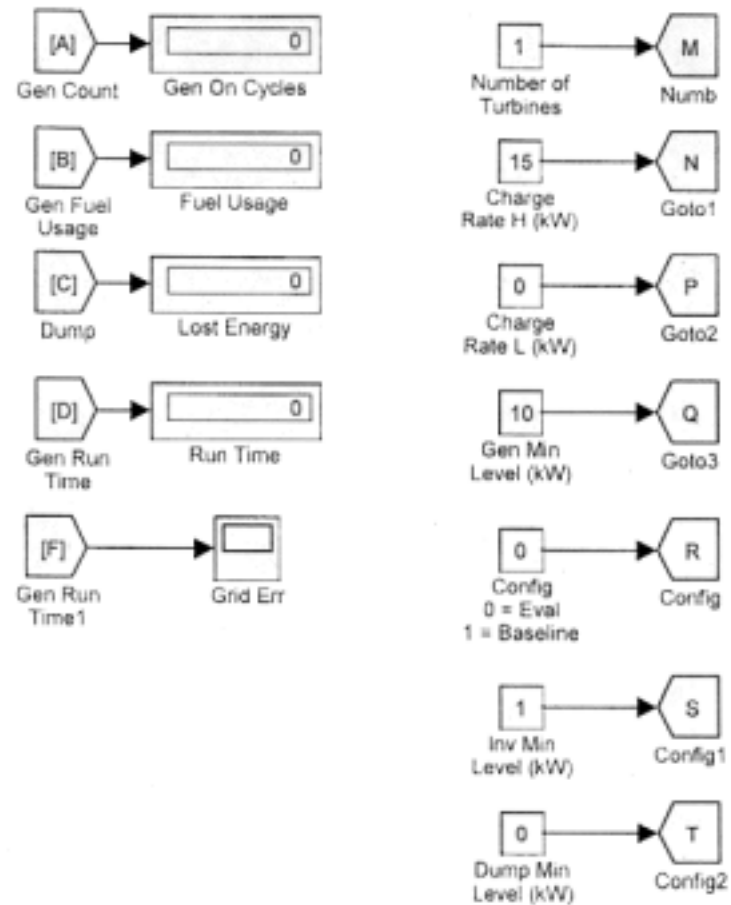
Update Time: 1.0 = 1.0 sec.

Version 5.0
Rev. # 0.0
Date 11/08/99



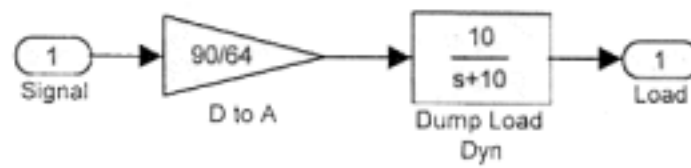
* NOTE: Negative Gen/Inv output is defined as power to the grid

NREL Modified Inverter Model Input/Output Control Panel



Ver 4.0 Added min Inv Load for dump load Controller
 Rev 1.0 Change Discharge to Charge (high)
 Rev 3.0 Added minimum dump load value

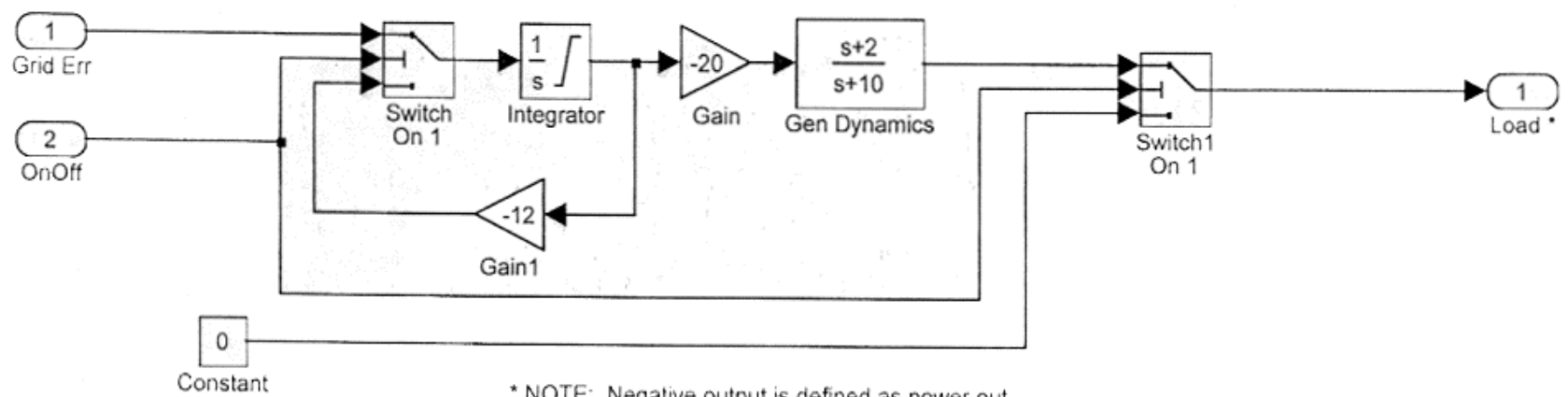
Dump Load Model



Rev 1.0 Changed max dump load to 90 kW

Generator Model

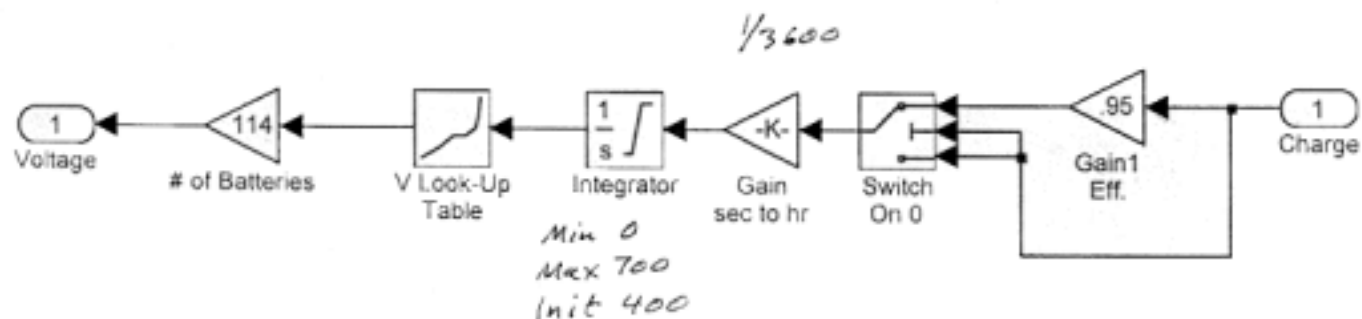
Min = 0
Max = 80



* NOTE: Negative output is defined as power out

Rev1: Removed Rate Limiter to Investigate stability Issue

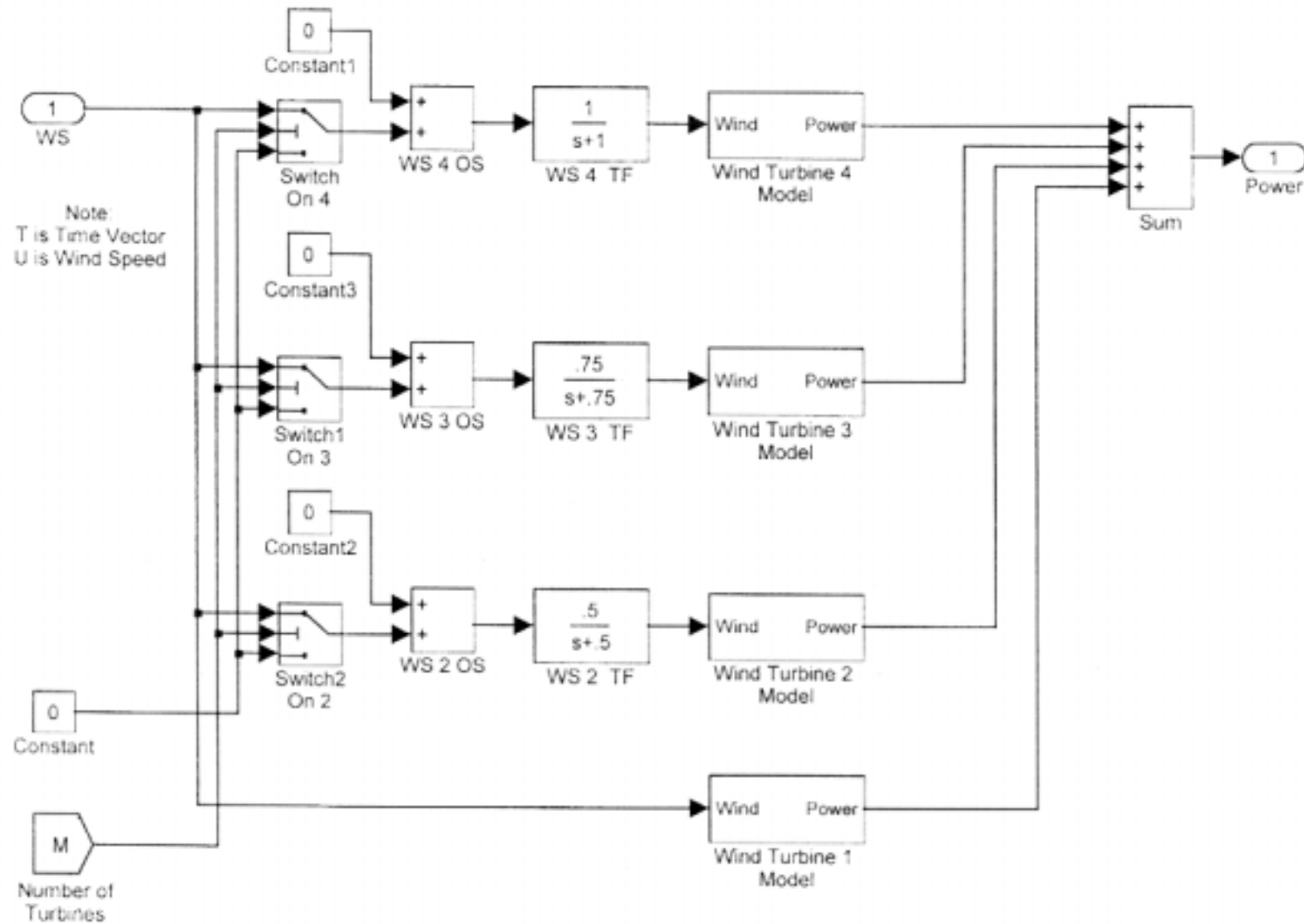
Battery Model



Ver 2.0 Change values for NREL H/W (Battery Model)
Rev 1.0 Change # Batteries to 114

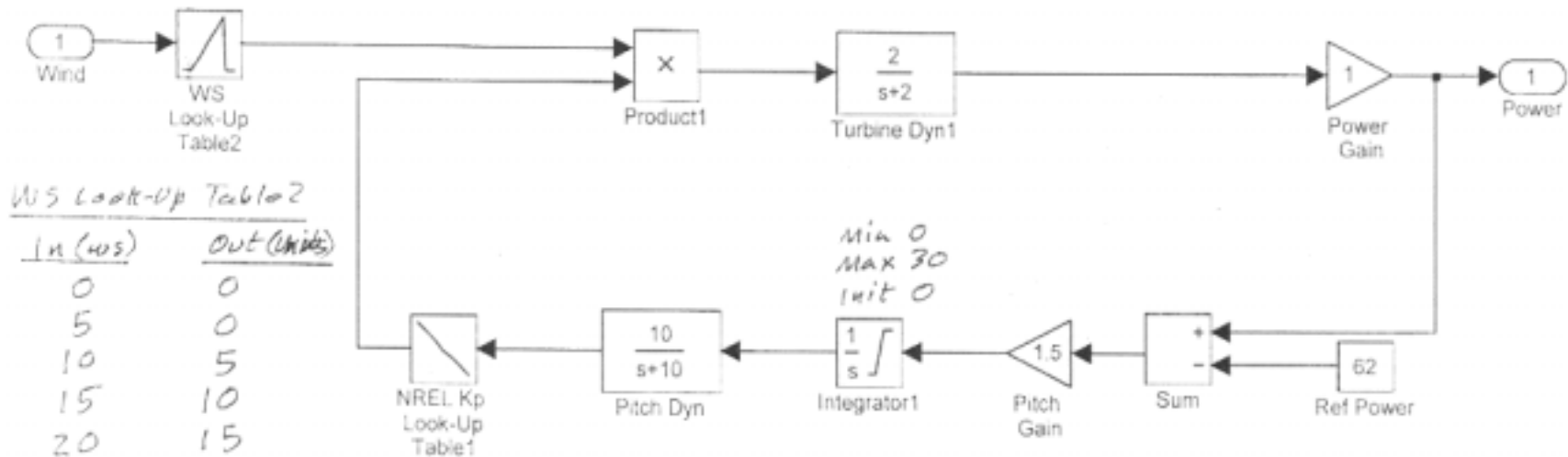
<u>V Look-Up Table</u>		
<u>Amp-hrs</u>	<u>Volts/cell</u>	<u>Volts (Res)</u>
0	1.6	182.4
195	1.8	205.2
390	2.03	231.4
520	2.07	236.0
650	2.20	250.8
675	2.40	273.6
700	2.80	319.2

Wind Plant Simulation



Rev 3: Added offset to windspeed inputs to turbines #2, 3, and 4

Wind Turbine1 Model



WS Look-Up Table 2

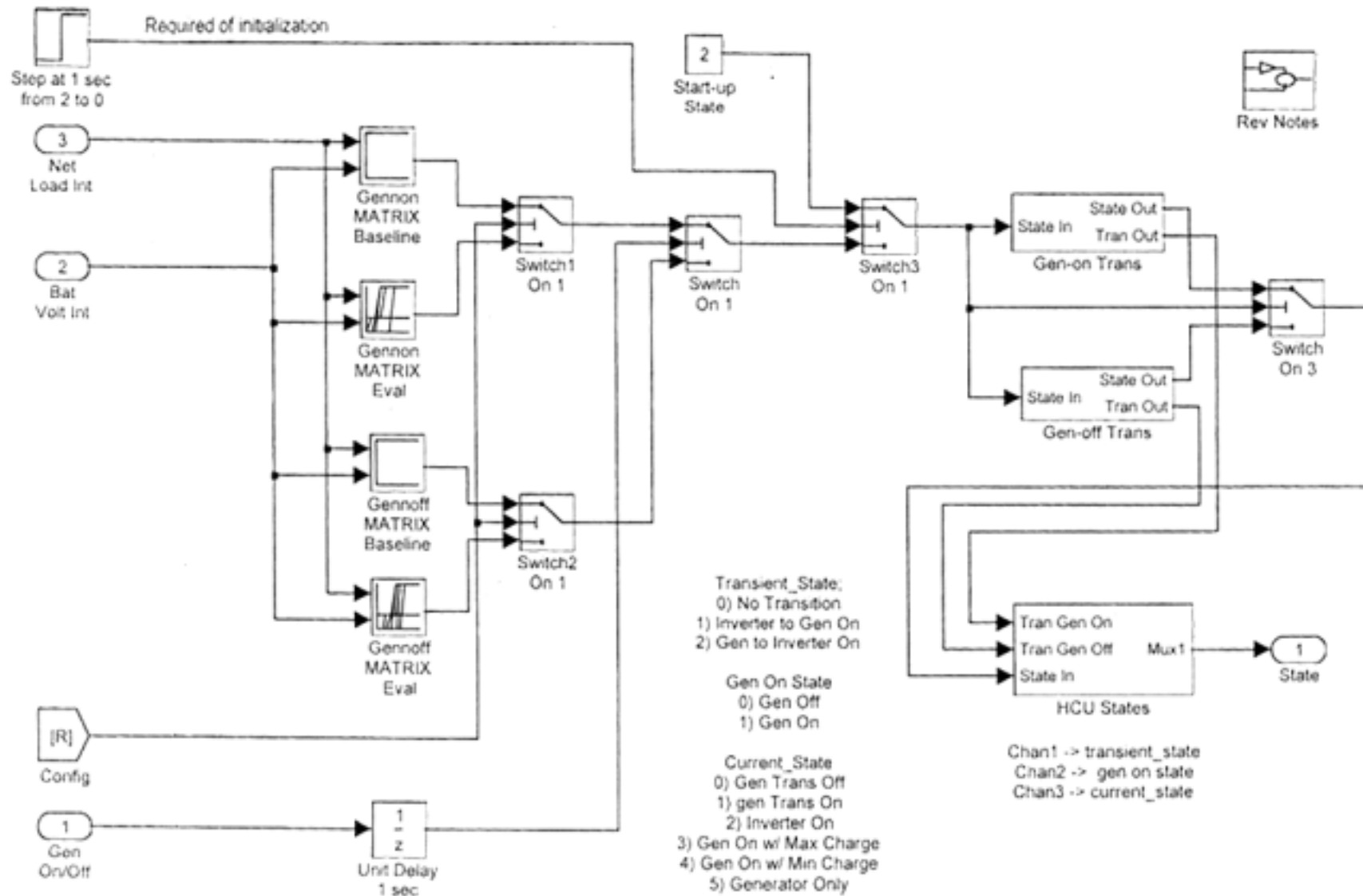
In (ws)	Out (Units)
0	0
5	0
10	5
15	10
20	15
24	19
25	0
30	0

NREL Kp Look-Up Table 1

In (Pitch Angle)	Out (Kp)
0	6.2
5	5.4
10	4.6
15	3.8
20	3.1
25	2.3
30	1.6

Simple NREL Wind Turbine Model
 Linear Power from 5 mps to 15 mps
 Rated at 62 kW
 For a step 0 to 20 mps; ~ 85 kW peak, settling time ~ 4 sec

Matrix Logic



MXEVOFF1 Desired State MATRIX for Evaluation Gen Off (Rev 1)

8/4/99

Net Load	Battery State of Charge (SOC)									
	1	2	3	4	5	6	7	8	9	10
0	3	2	2	2	2	2	2	2	2	2
1	3	2	2	2	2	2	2	2	2	2
2	3	3	3	2	2	2	2	2	2	2
3	3	3	3	3	2	2	2	2	2	2
4	3	3	3	5	5	5	5	5	2	2
5	3	3	5	5	5	5	5	5	5	2
6	3	3	5	5	5	5	5	5	5	5
7	3	3	5	5	5	5	5	5	5	5
8	3	3	5	5	5	5	5	5	5	5
9	3	3	5	5	5	5	5	5	5	5

MXEVON1 Desired State MATRIX for Evaluation Gen On (Rev 1)

Net Load	Battery State of Charge (SOC)									
	1	2	3	4	5	6	7	8	9	10
0	3	3	2	2	2	2	2	2	2	2
1	3	3	3	2	2	2	2	2	2	2
2	3	3	3	3	3	2	2	2	2	2
3	3	3	5	5	5	5	5	5	5	2
4	3	5	5	5	5	5	5	5	5	2
5	3	5	5	5	5	5	5	5	5	2
6	3	5	5	5	5	5	5	5	5	5
7	3	5	5	5	5	5	5	5	5	5
8	3	5	5	5	5	5	5	5	5	5
9	3	5	5	5	5	5	5	5	5	5

Note: State ≤ 2 Gen Off States
 State ≥ 3 Gen On States

5 = Gen only

MXBLOFF1 Desired State MATRIX for Baseline Gen Off (Rev 1)

NET Load	Battery Capacity (SOC)									
	1	2	3	4	5	6	7	8	9	10
0	3	2	2	2	2	2	2	2	2	2
1	3	2	2	2	2	2	2	2	2	2
2	3	2	2	2	2	2	2	2	2	2
3	3	2	2	2	2	2	2	2	2	2
4	3	2	2	2	2	2	2	2	2	2
5	3	2	2	2	2	2	2	2	2	2
6	3	2	2	2	2	2	2	2	2	2
7	3	2	2	2	2	2	2	2	2	2
8	3	2	2	2	2	2	2	2	2	2
9	3	2	2	2	2	2	2	2	2	2

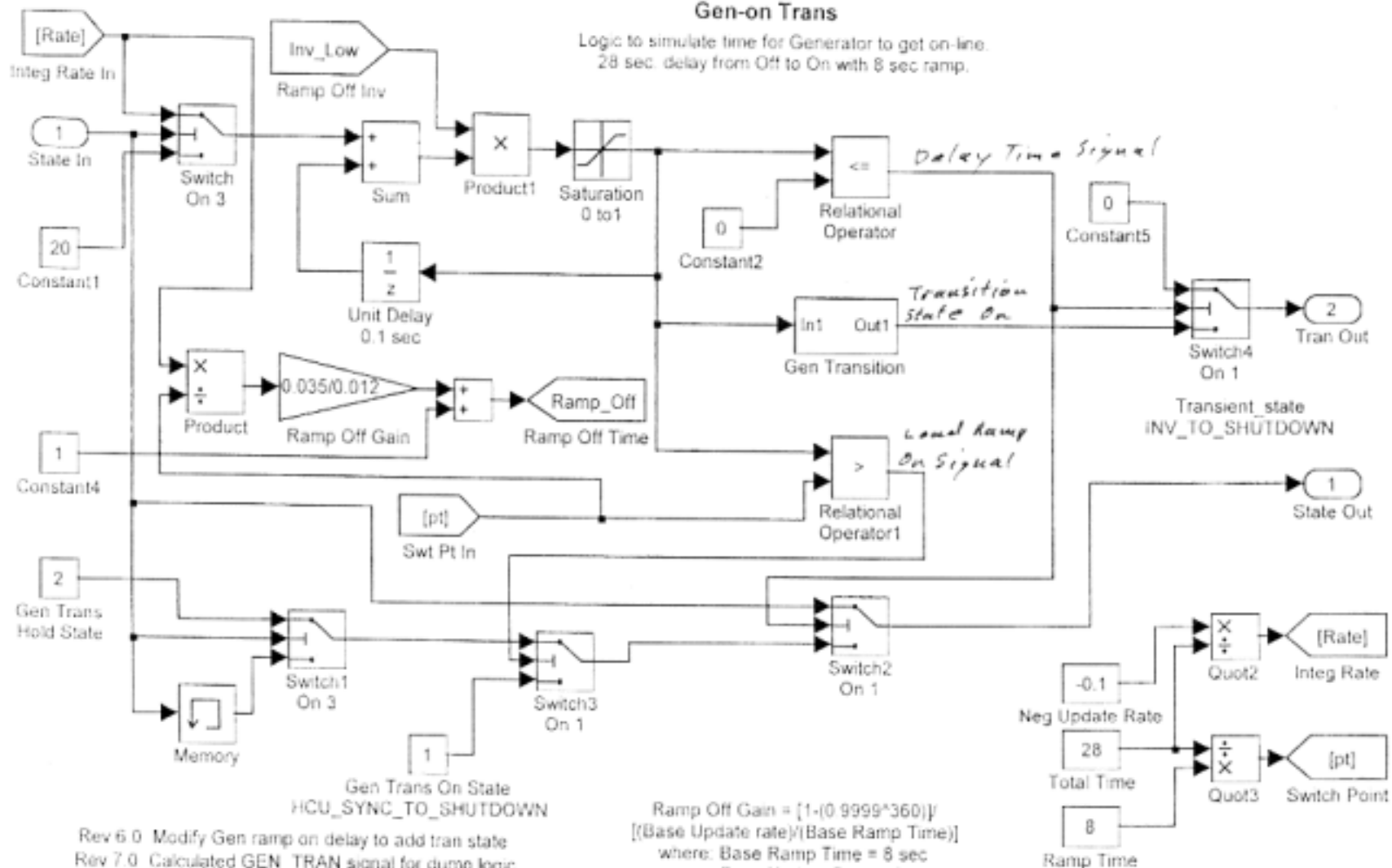
MXBLON1 Desired State MATRIX for Baseline Gen On (Rev 1)

NET Load	Battery Capacity (SOC)									
	1	2	3	4	5	6	7	8	9	10
0	3	3	3	3	3	3	3	3	3	2
1	3	3	3	3	3	3	3	3	3	2
2	3	3	3	3	3	3	3	3	3	2
3	3	3	3	3	3	3	3	3	3	2
4	3	3	3	3	3	3	3	3	3	2
5	3	3	3	3	3	3	3	3	3	2
6	3	3	3	3	3	3	3	3	3	2
7	3	3	3	3	3	3	3	3	3	2
8	3	3	3	3	3	3	3	3	3	2
9	3	3	3	3	3	3	3	3	3	2

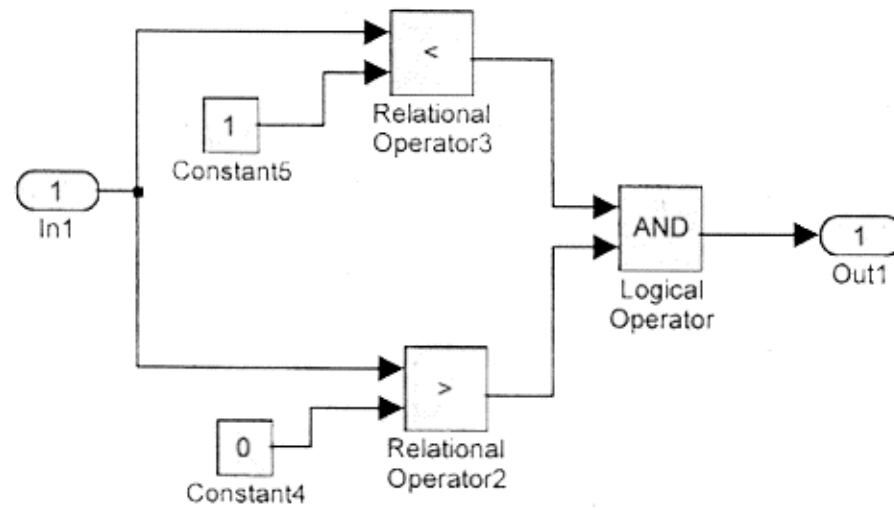
Note: State ≤ 2 Gen Off States
State ≥ 3 Gen On States

Gen-on Trans

Logic to simulate time for Generator to get on-line.
28 sec. delay from Off to On with 8 sec ramp.

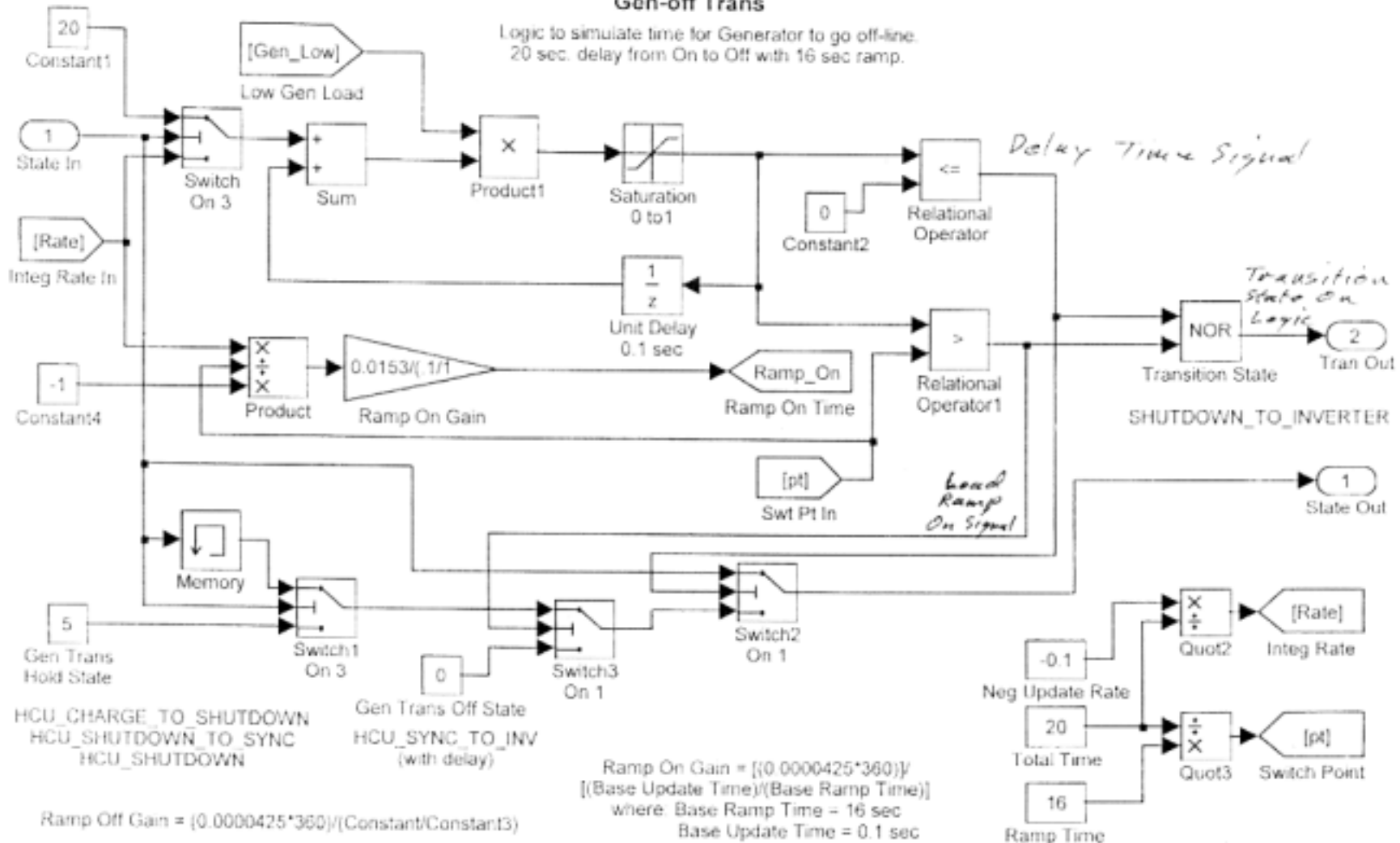


Gen Transition



Gen-off Trans

Logic to simulate time for Generator to go off-line.
20 sec. delay from On to Off with 16 sec ramp.



Ramp Off Gain = $\{(0.0000425 \times 360) / (Constant/Constant3)\}$

Rev 6.0 Modify Gen ramp on delay to add tran state

Rev 8.0 Added Ramp_On calc to automate trans. load

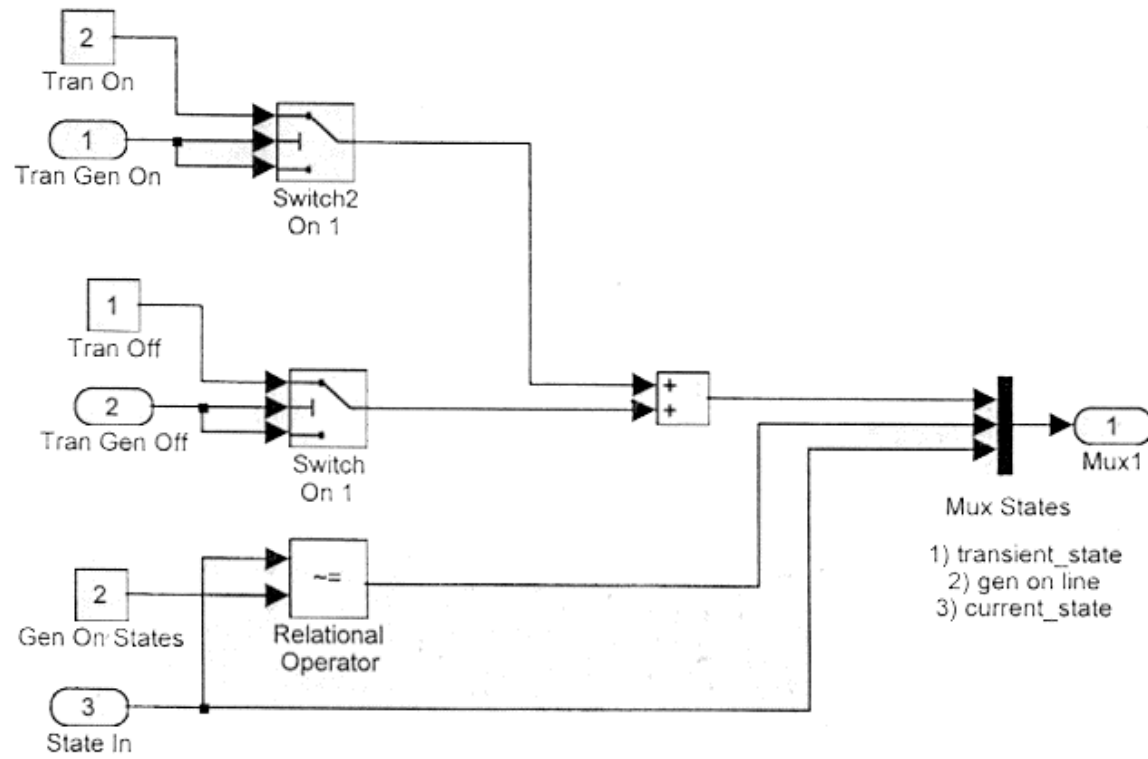
Rev 9.0 Added Transition state calc/output SHUTDOWN_TO_INVERTER

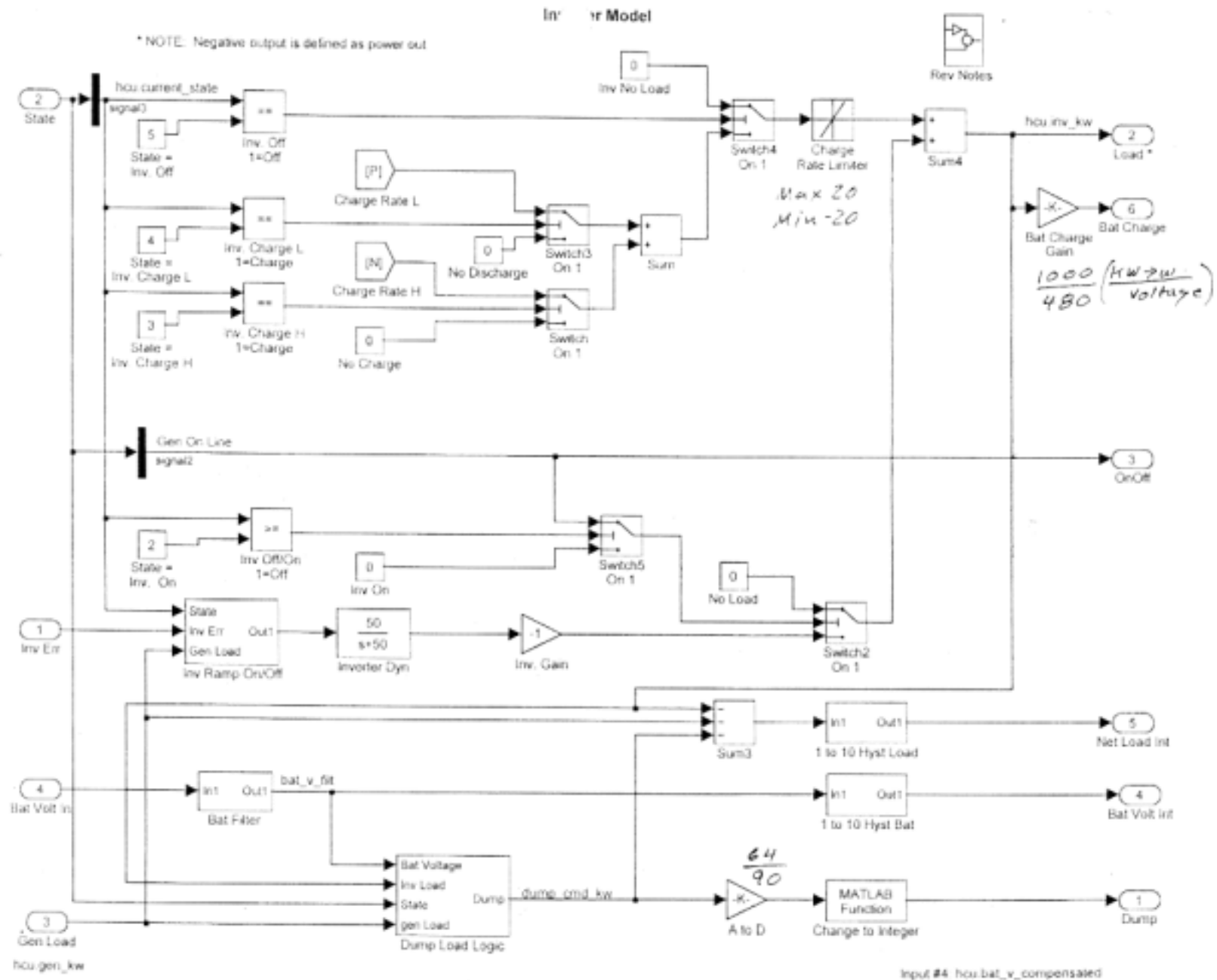
Ver 5.0 Moved location of Gen_Low transition logic

Ver 5.0 Modified On Rate time variable inputs (simplify)

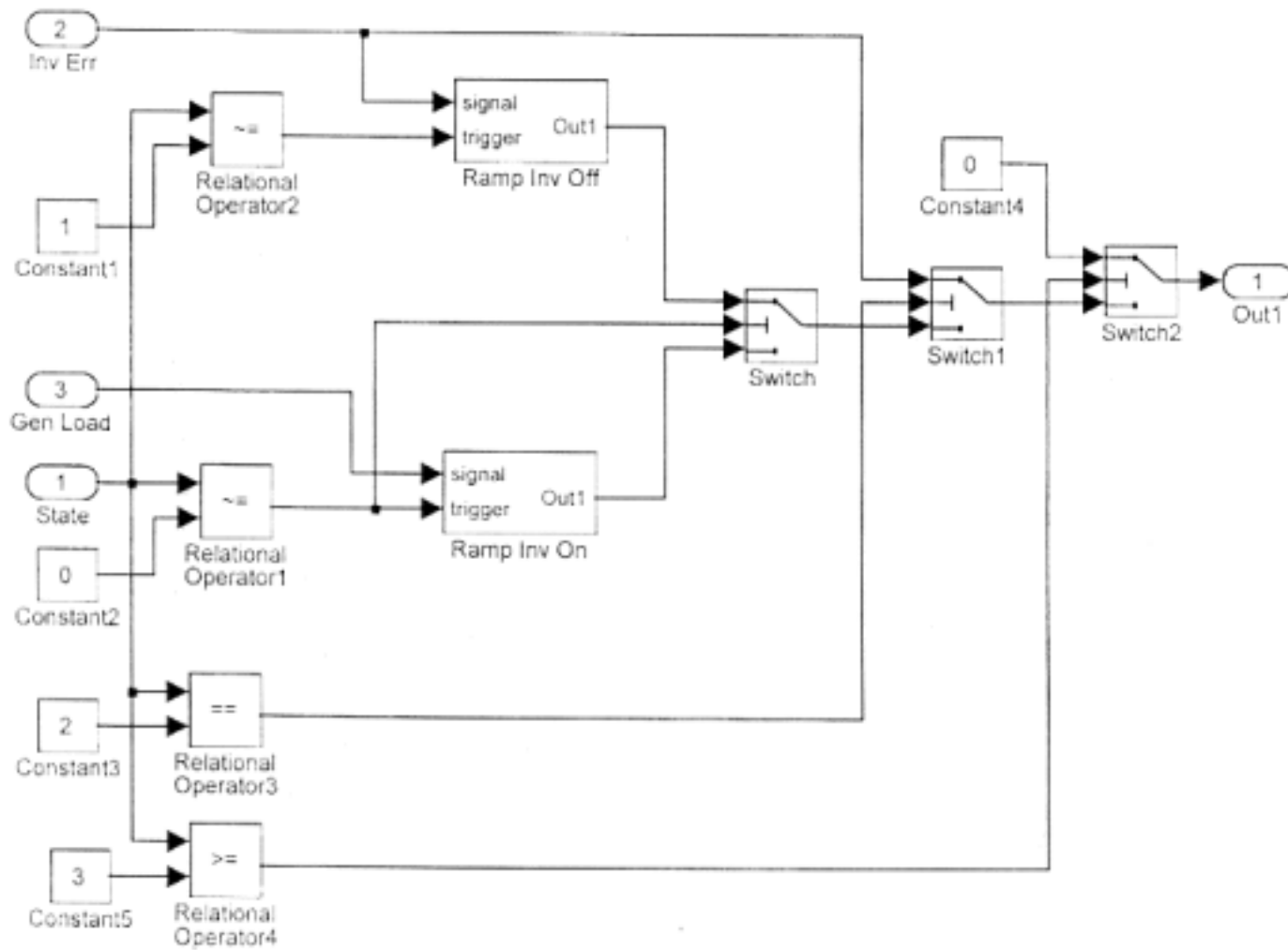
[Rate] = Ramp on time rate step
-0.005 @ 0.1 sec update = 20 sec delay
[pt] = Transition threshold to ramp load
with 4 sec delay, 0.8 = 16 sec ramp

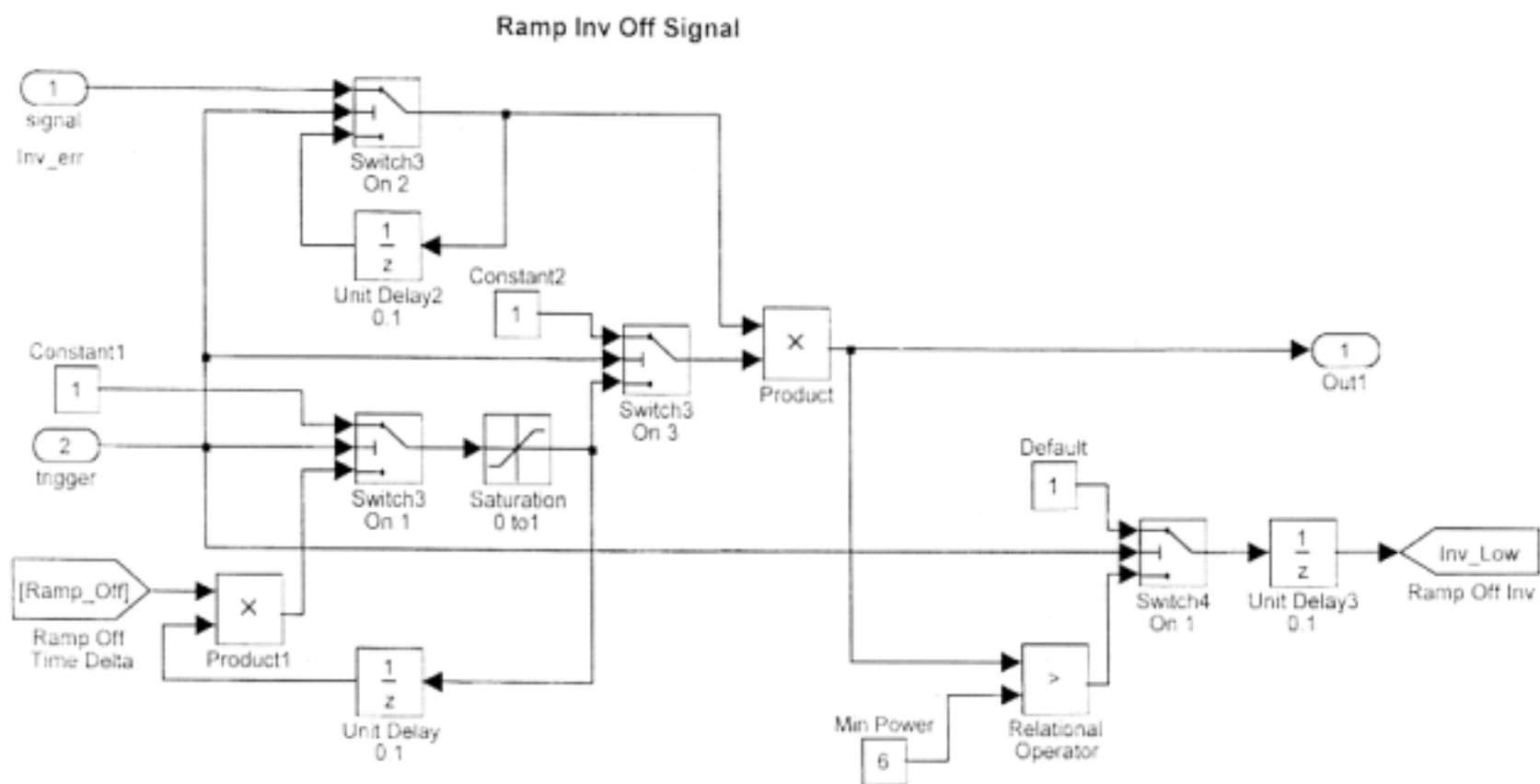
HCU States





Inv Ramp On/Off

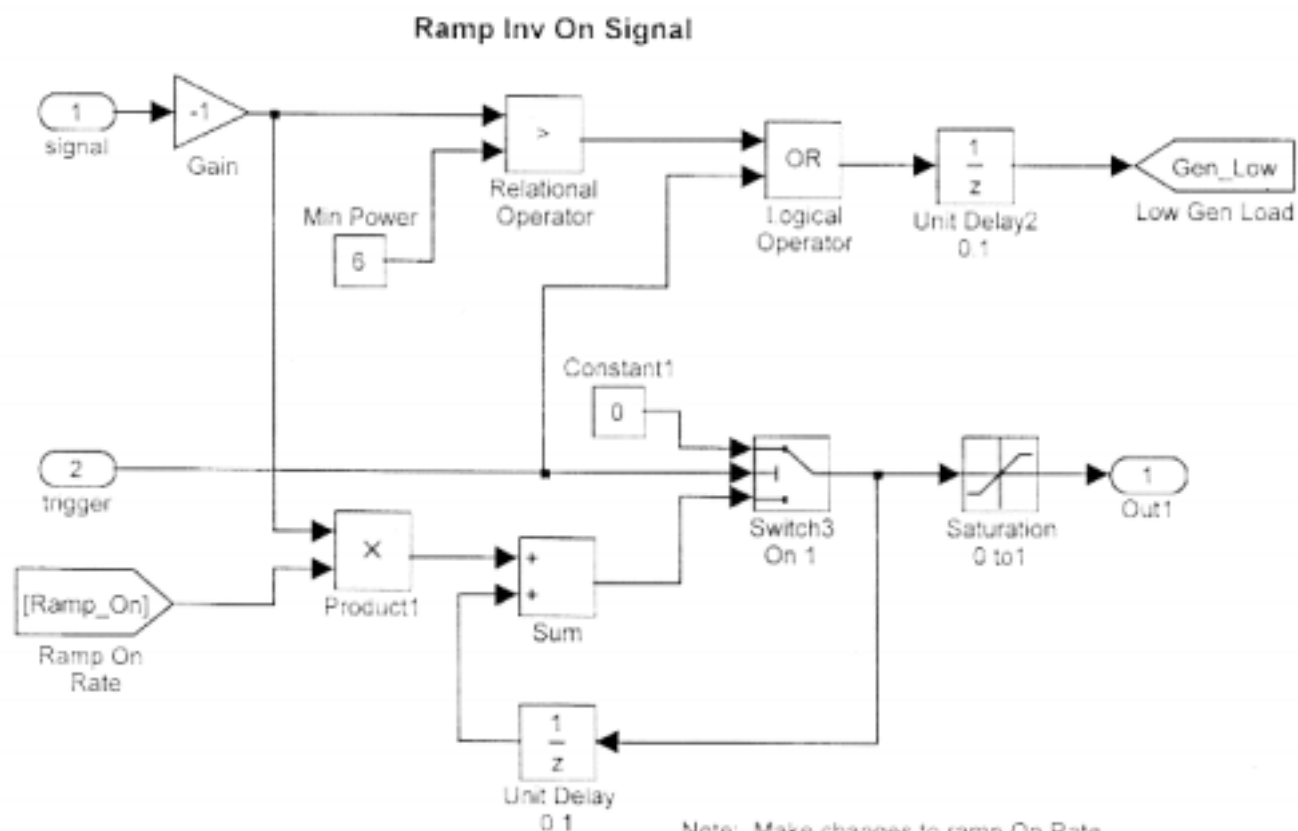




Note: Make changes to ramp time delay with "Gen-Off Trans" function

Rev 8.0 Added Ramp_Off signal to set load transfer rate

Ver 5.0 Added Inv_Low Calc and mod ramp off logic



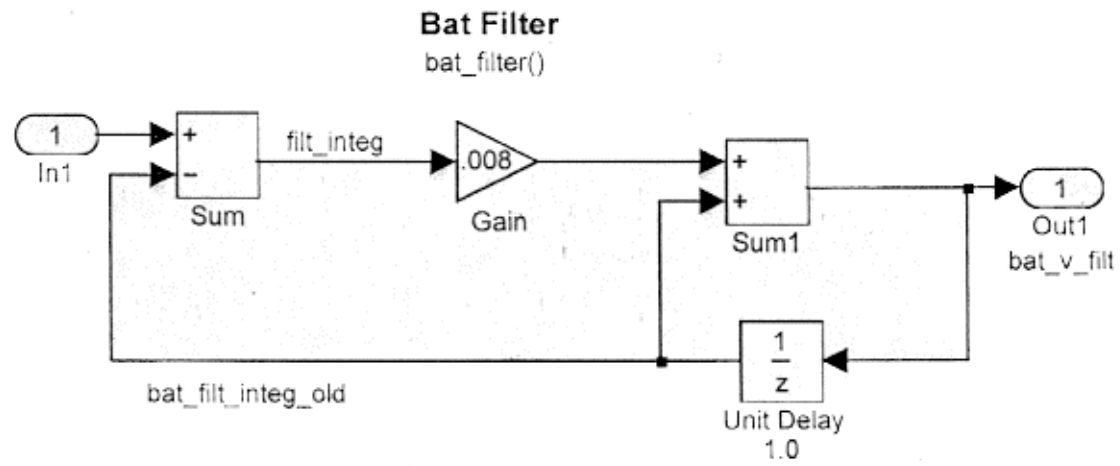
Note: Make changes to ramp On Rate
with "Gen-On Trans" function

Rev 8.0 Added Ramp_On signal to set load transfer rate

Rev 8.0 Calc Gen_Low signal to determine min gen load during transfer of load

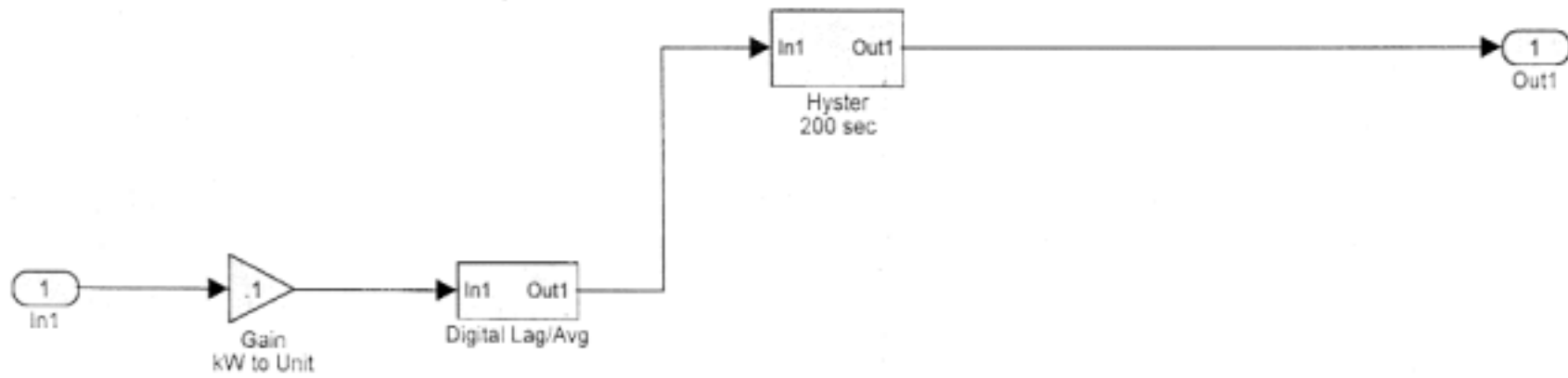
Rev 8.0 Added delay to Gen_low signal to address algebraic loop

Ver 5.0 Changes sense of Gen_low signal and added state lockout



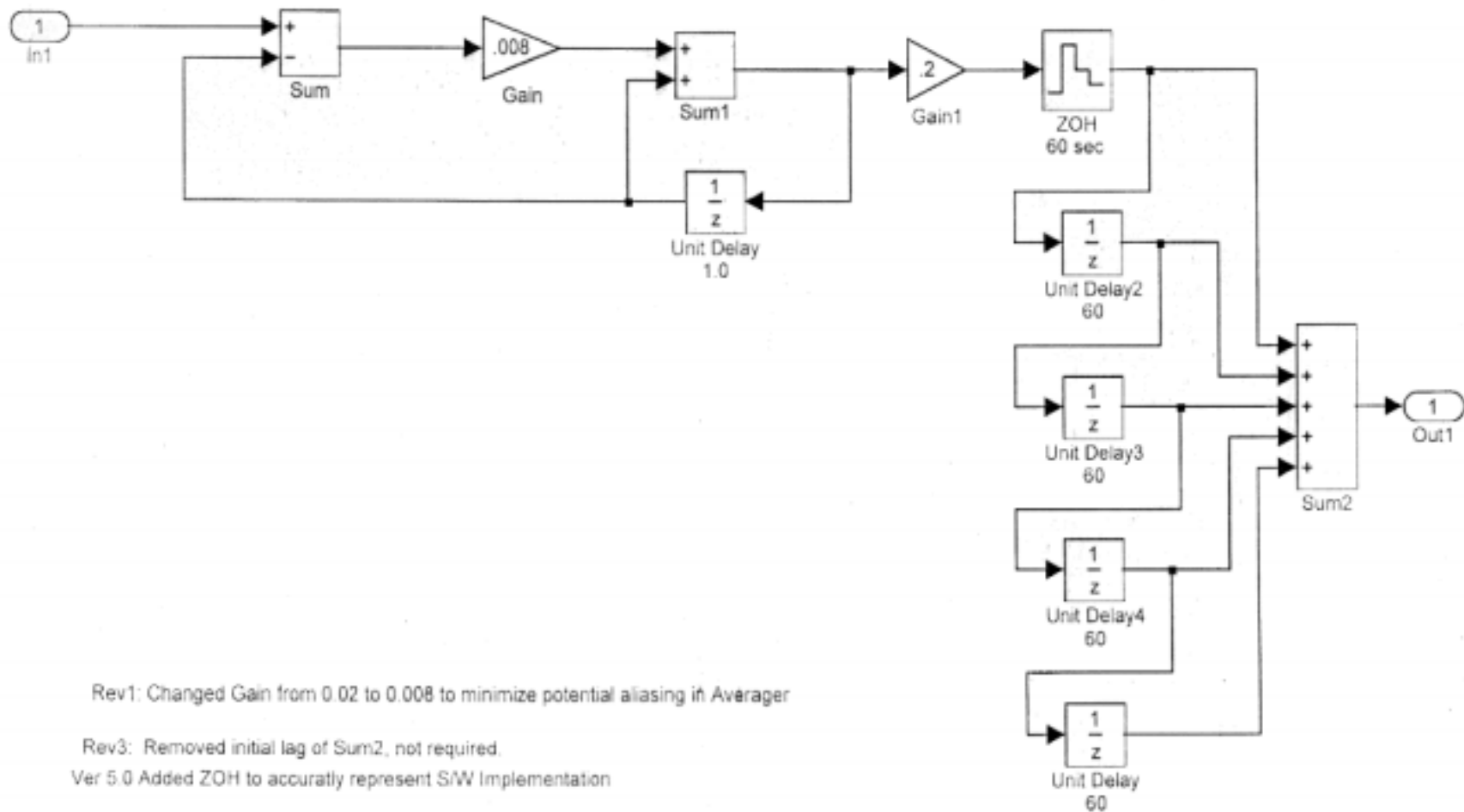
~125sec Time Constant

1 to 10 Hyst Load



Rev 3: Changed First order lag (4 Step Lag) function to discrete implementation (Digital Lag)

Digital Lag/Avg



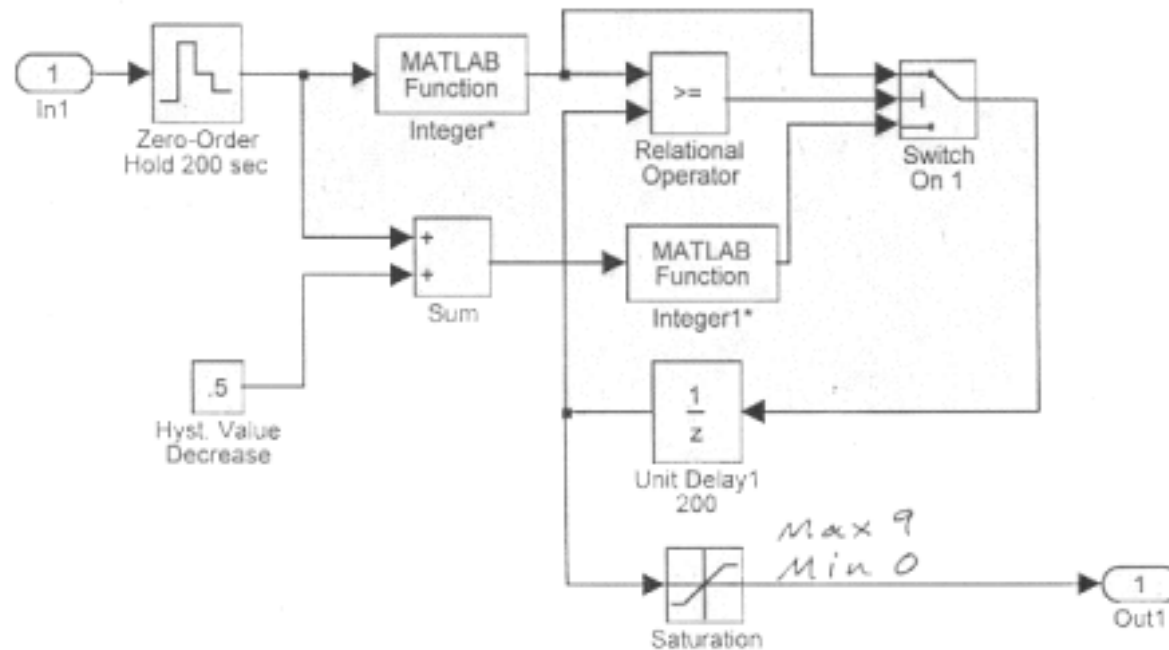
Rev1: Changed Gain from 0.02 to 0.008 to minimize potential aliasing in Averager

Rev3: Removed initial lag of Sum2, not required.

Ver 5.0 Added ZOH to accurately represent S/W Implementation

Hyster 200 sec

(Float to Integer Conversion with hysteresis)



* NOTE: Float to Integer Conversion

Rev 1.0 Change Saturation Limits to 0 to 9

Rev 4.0 Changed Load Hyster input delay to 200 sec ZOH & output delay to 1 sec

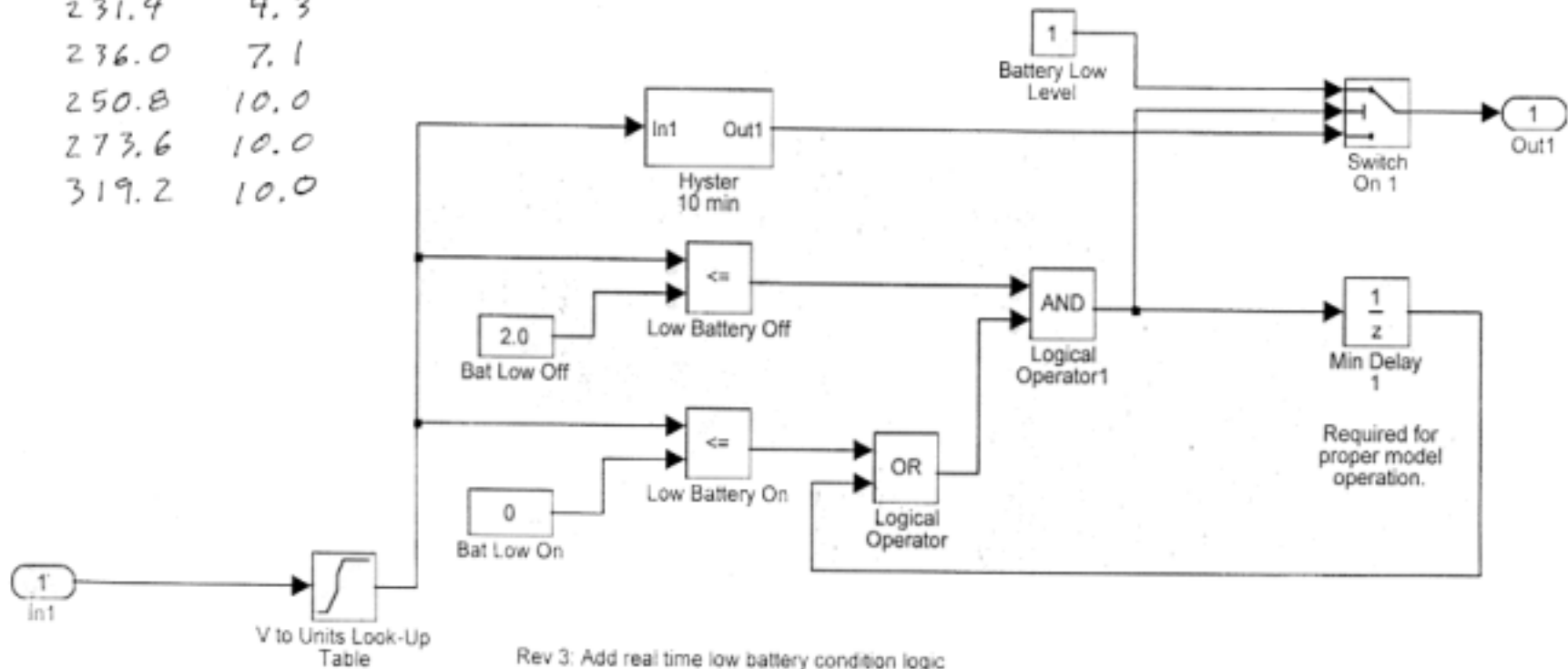
Ver 5.0 Changed Net Load Unit Delay to 200 sec

V to Units Look-Up Table

In (volts) Out (soc)

182.4	0.0
205.2	0.0
231.4	4.3
236.0	7.1
250.8	10.0
273.6	10.0
319.2	10.0

1 to 10 Hyst Bat



Rev 3: Add real time low battery condition logic

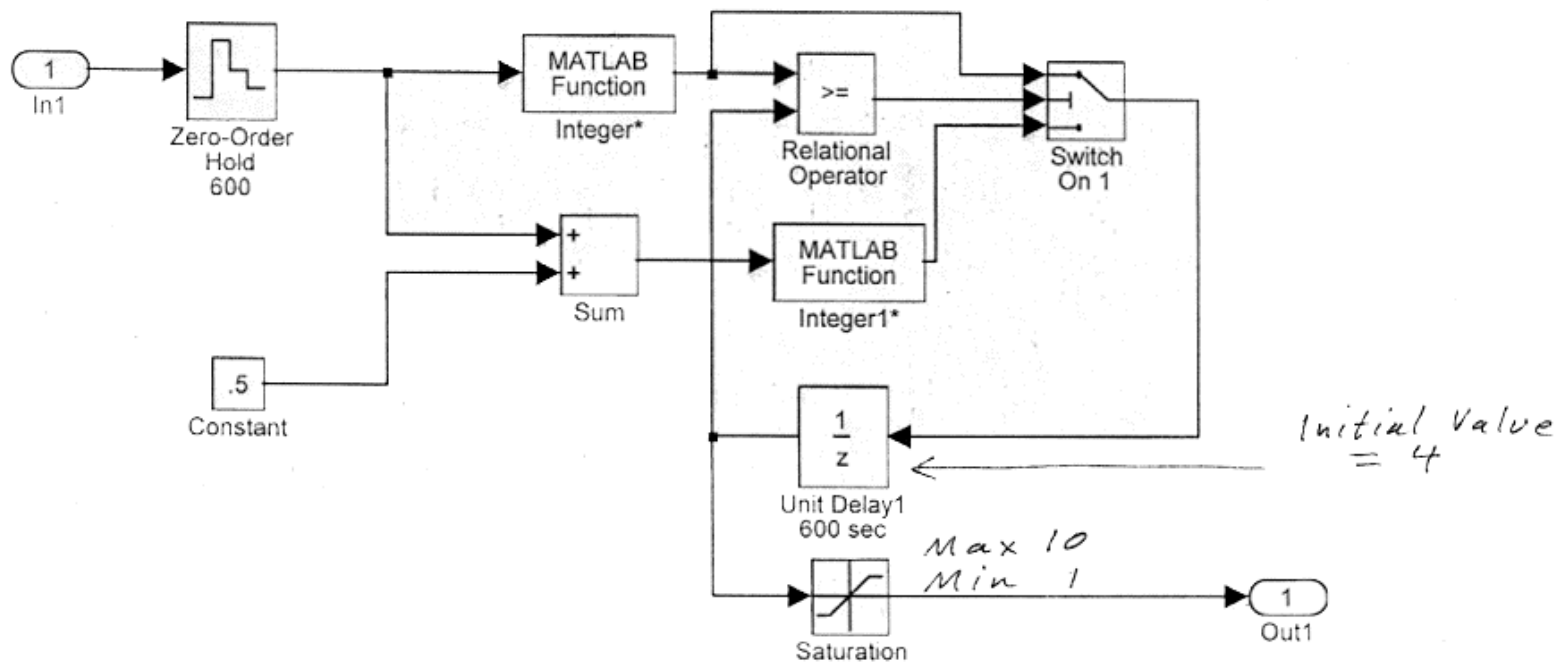
Ver 2.01 to 6 Hyst Bat: Modify for NREL H/W (Battery Voltage to Storage)

Rev 1.0 Changed V to Units Table for new # of cells (100 to 114)

Rev 4.0 Changed Battery Hyster input delay to 600 sec ZOH & output delay to 1 sec

Hyster 10 min

(Float to Integer Conversion with hysteresis)

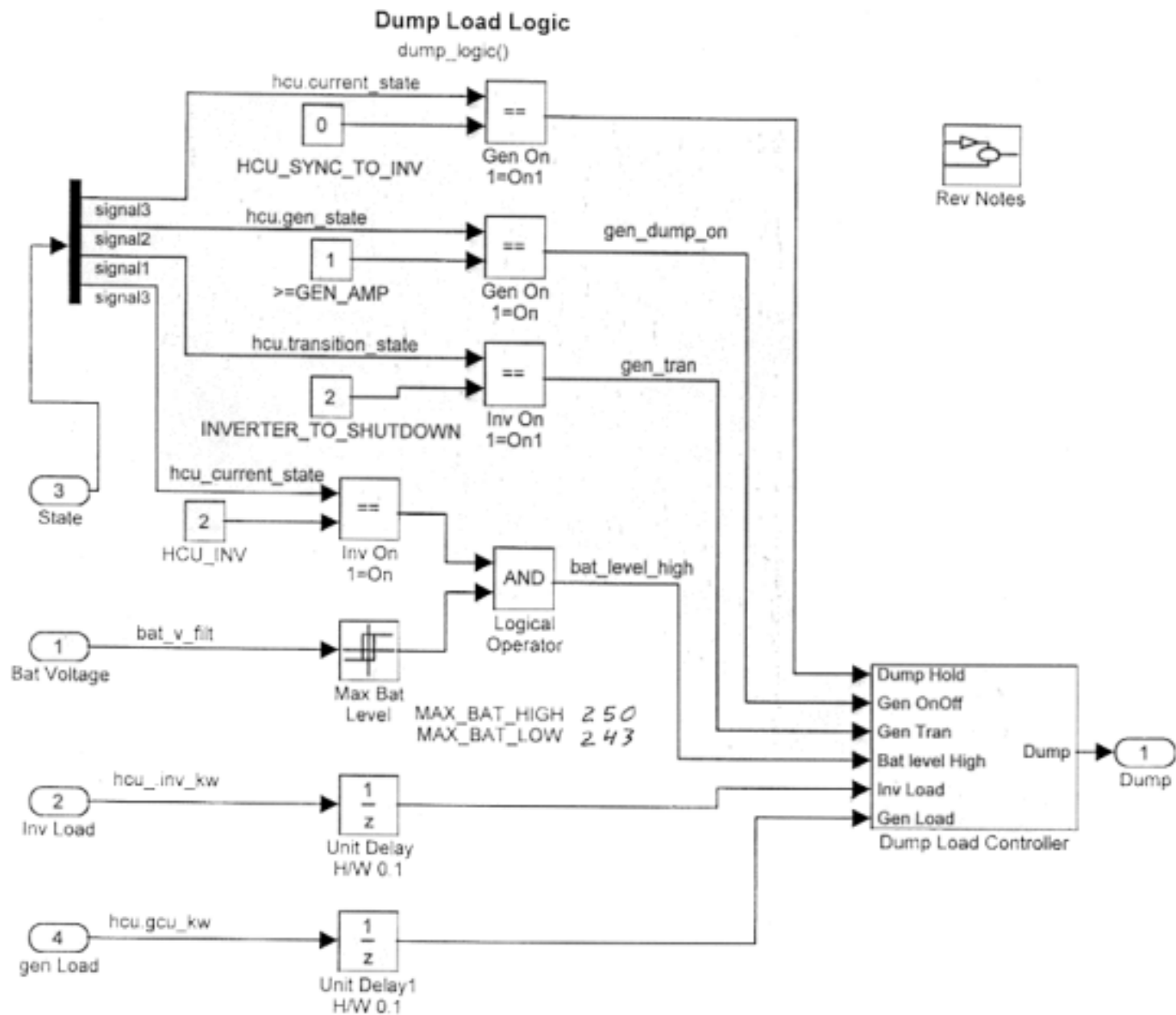


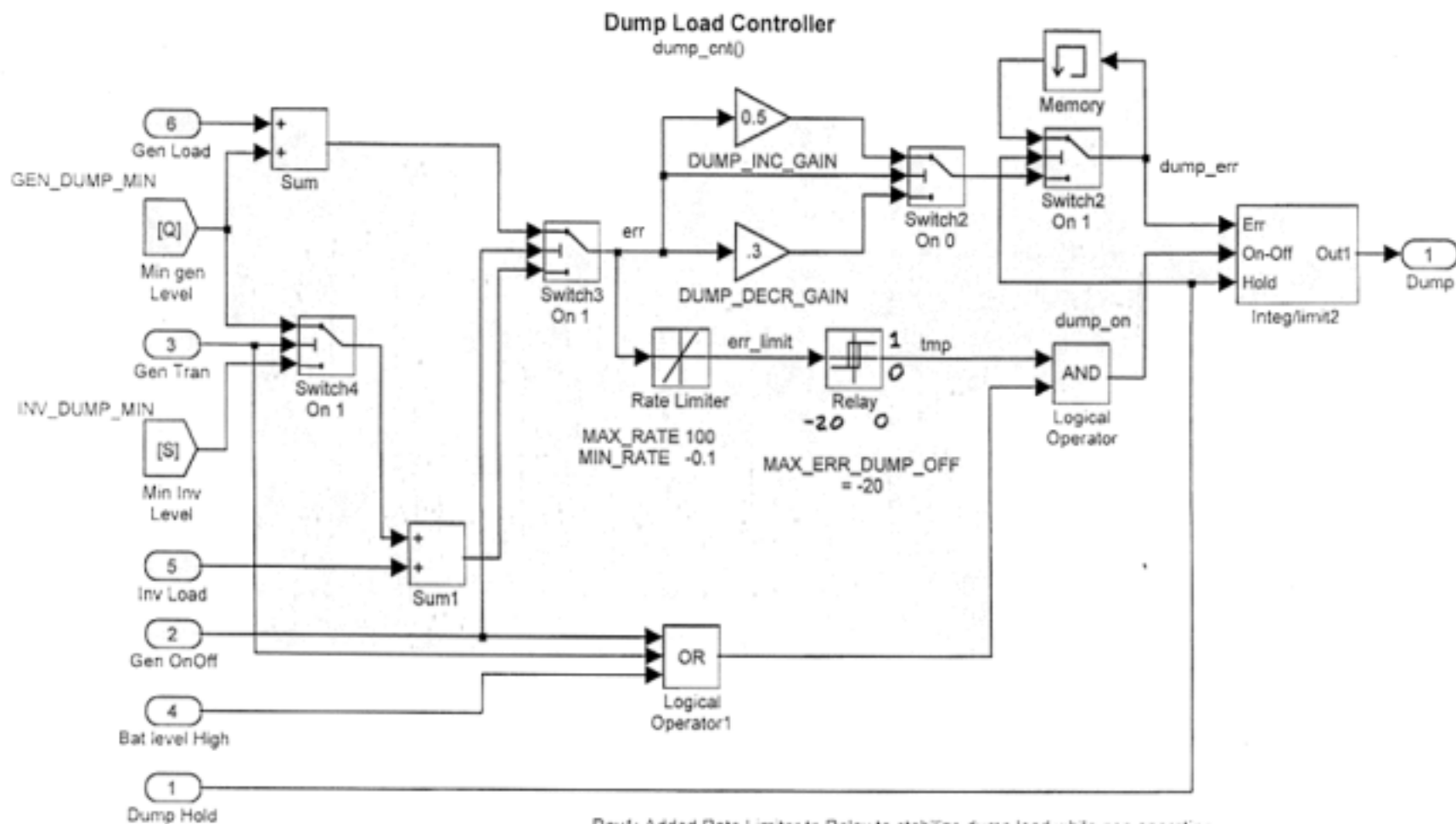
* NOTE: Float to Integer Conversion

Ver 2.0 Hyster: Update Unit Delay and Saturation Limits

Rev 4.0 Changed Battery Hyster input delay to 600 sec ZOH & output delay to 1 sec

Ver 5.0 Changed Battery Hyst Unit Delay to 600 sec





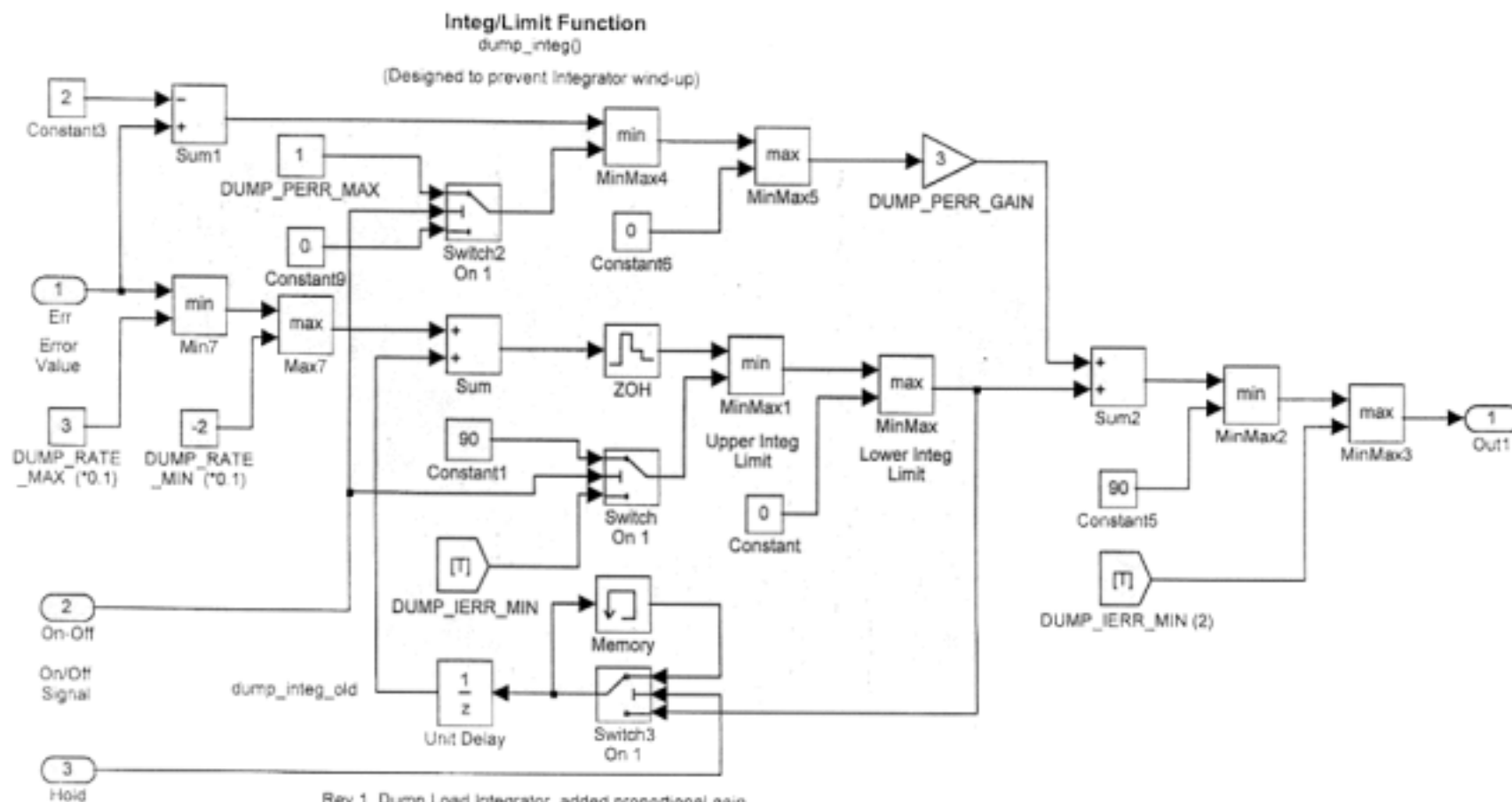
Rev1: Added Rate Limiter to Relay to stabilize dump load while gen operating

Ver 4.0 Changed 'Inv err signal' to Inverter 'load' value & required Dump Load controller changes

Rev 2.0 Added gen transition on logic to dump load

Rev 7.0 Changed DUMP_DECR_GAIN to 0.3

Rev 7.0 Added hold function to Integ/limit1 function



Rev 1 Dump Load Integrator, added proportional gain

Rev3: Modified Dump Load Integ/Limit function (added proportional gain term and mod rate limits)

Rev 3.0 Added minimum dump load value

Rev 7.0 Changed DUMP_RATE_MIN to -20

Rev 7.0 Changed DUMP_PERR_GAIN to 3.0 due to faster gen dynamics

Ver 5.0 Modified Integrator Rate limits and added ZOH (better simulate actual code)

SIMULINK Diagrams of Dispatch Transient Model

Model Name: "nreltrn6.mdl" Version 6.0 Rev 0

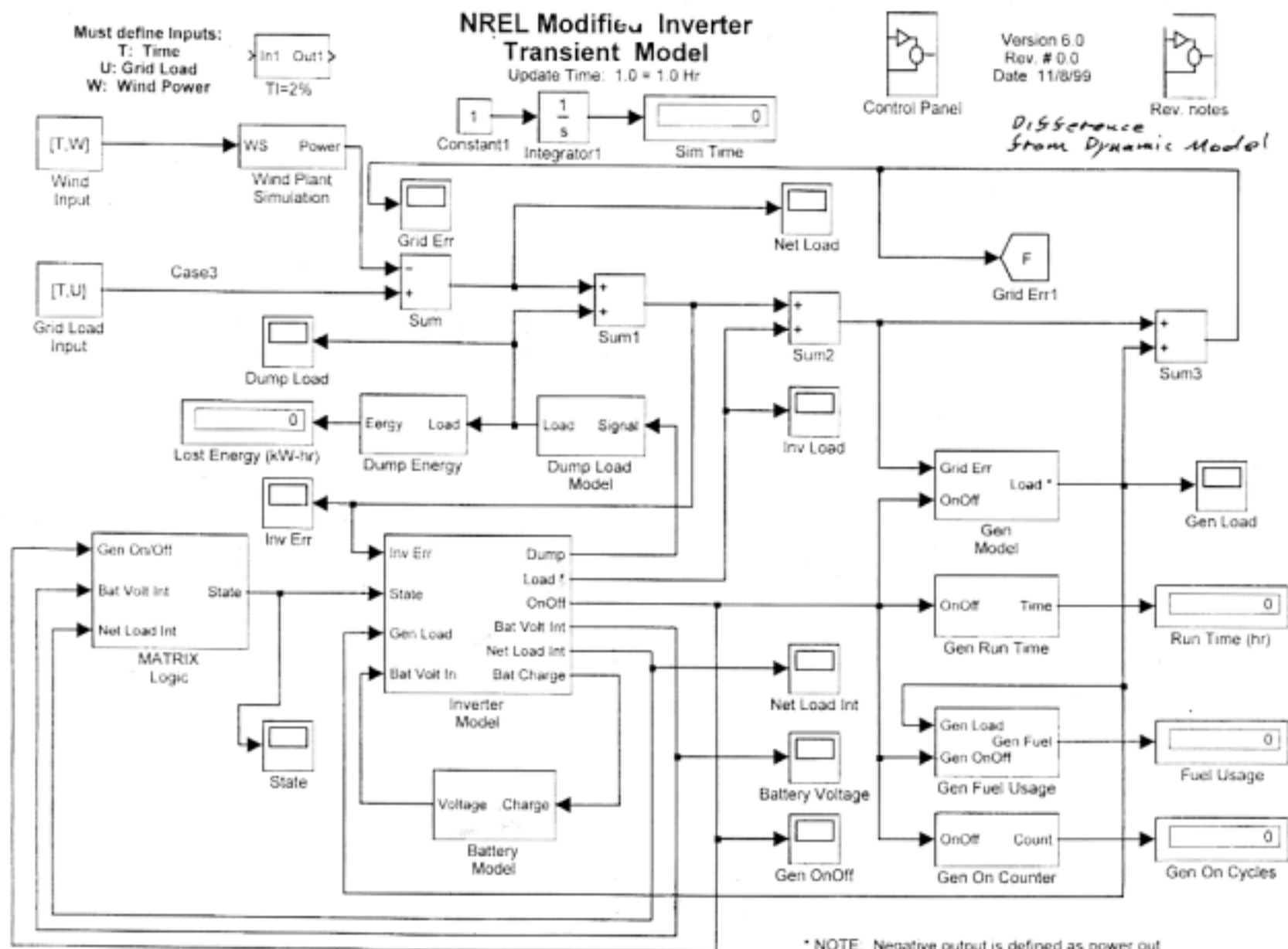
NREL Modified Inverter Model Revision Notes

Version 1.0 Baseline

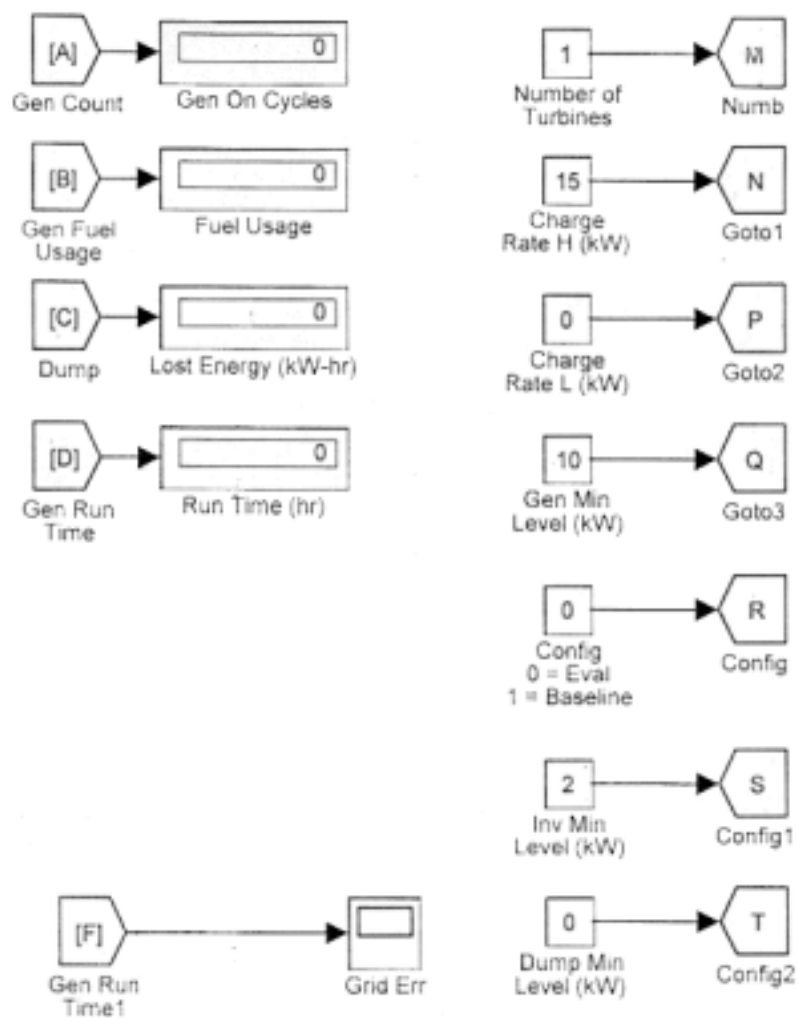
- Rev 1: Changed 0 to 6 Hyst Logic, in Inverter Model, to simulate C code implementation
- Rev 2: Integrator Limit mod for C code implementation
- Rev 2: Changed Inc rate from 2.0 to 0.02 & Dec rate from 0.3 to 0.003
- Rev 2: Added step function to force start-up in Inverter mode, Required due to unit step delays in hyst function
- Rev 2: Changed MATRIX Genon(1,3) from 3 to 2
- Rev 3: Changed First order lag (4 Step Lag) function to discrete implementation (Digital Lag)
- Rev 3: Updated wind turbine model for TSR input to Kp Table
- Rev 3: Added offset to windspeed inputs to turbines #2,3 and 4
- Rev 3: Modified turbine logic to divide power delta by speed to get torque into integrator
- Rev 3: Added Ref Speed to properly calculate output power
- Rev 3: Add real time low battery condition logic

Version 3.0 Baseline Transient Model

- Ver 3.0 Modified Model to remove dynamics to change time step to 1.0 = 1.0 hour. Improve run time.
- Ver 3.0 Modified Wind Turbine Model to Simplified Power Curve
- Ver 3.0 Modified Dump Logic to use Gen Load and Net Err. directly
- Ver 3.0 modified MATRIX tables to ref. MXBLON, MXBLOFF, MXEVON, and MXEVOFF
- Ver 3.0 Updated Hysteresis to a time step of 1.0 = 1.0 hr
- Rev 1: Update to MATLAB Release 11
- Rev 2: Updated max dump load value to 90 kW
- Rev 2: Added min inverter load value
- Rev 2: Removed discharge and added charge L & charge H
- Rev 2: Change Net Load (row) saturation limits to 0 to 9 and update to new MATRIX tables
- Rev 2: Updated the V to Units Look-up Table
- Rev 2: Updated # of battery cells to 114
- Rev 2: Added Gen Transition on logic to dump load
- Rev 2: Modify the Max Bat Level Hyst. values due to change in # of battery cells
- Rev 2: Added battery filter
- Rev 3: Added min dump load value
- Ver 6.0 Rev 0.0 Update to Ver 5.0 Dynamic Model
- Ver 6.0 Set Gen Tran to Off
- Ver 6.0 Changed load delay to 200 sec ZOH
- Ver 6.0 Changed delay to 500 sec ZOH
- Ver 6.0 Removed delay1, not required
- Ver 6.0 Modified Gains for 1 hr update rate
- Ver 6.0 Added ZOH to accurately represent S/W Implementation
- Ver 6.0 Incorporated wind turbine simulation



NREL Modified Inverter Model Input/Output Control Panel

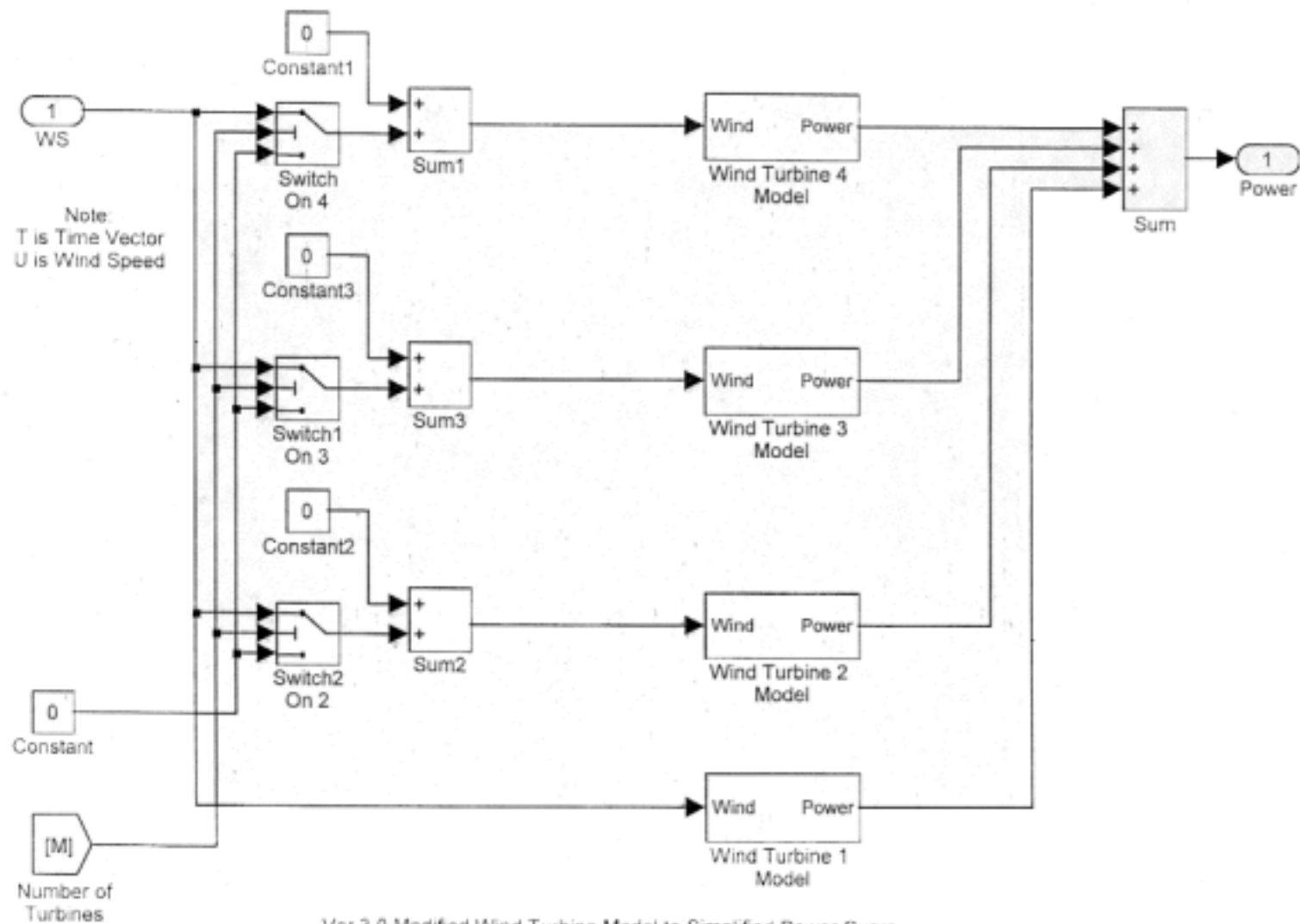


Rev 2: Added min inverter load value

Rev 2: Removed discharge and added charge L & charge H

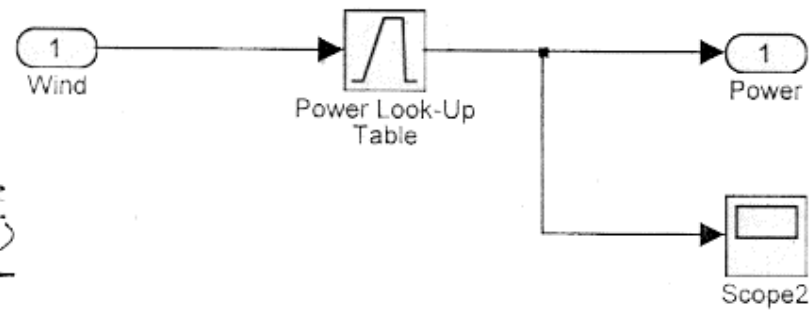
Rev 3: Added min dump load value

Wind Plant Simulation



Ver 3.0 Modified Wind Turbine Model to Simplified Power Curve

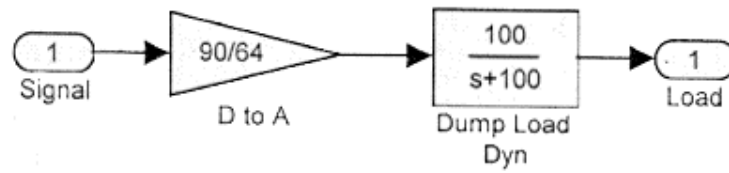
Wind Turbine Model



Power Look-Up Table

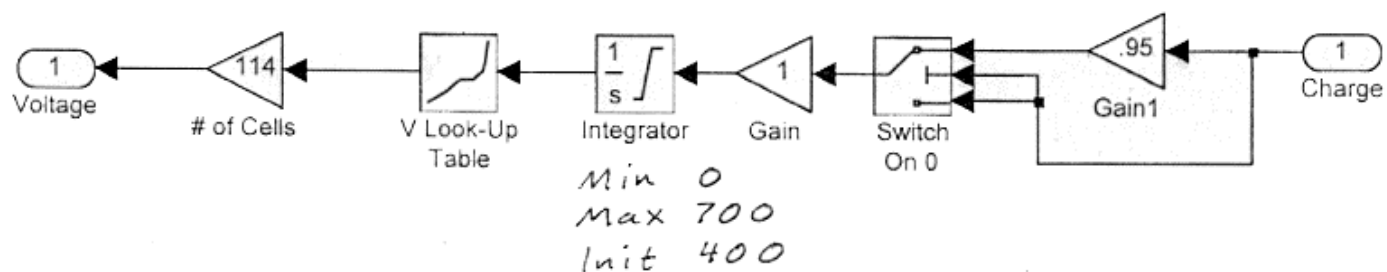
<i>In (mps)</i>	<i>Out (kW)</i>
0	0
5	0
15	62
20	62
24	62
25	0
30	0

Dump Load Model



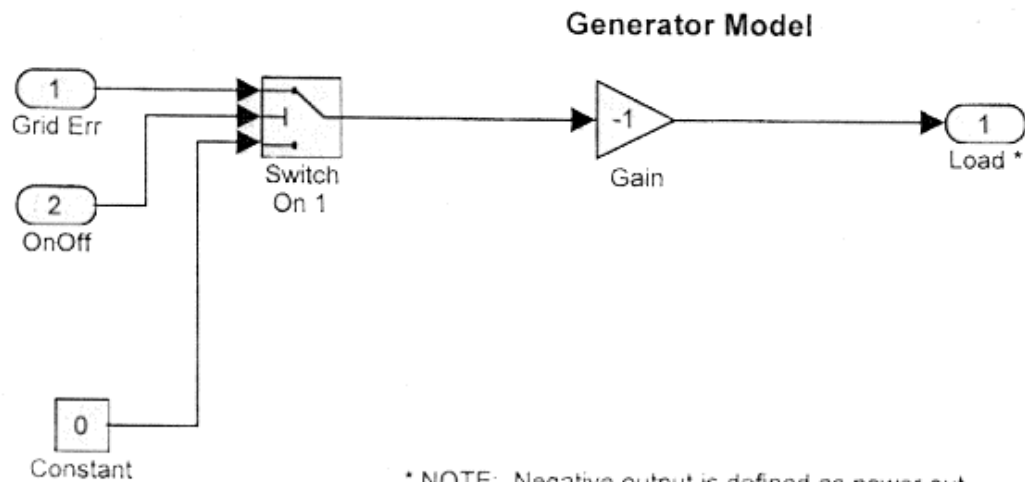
Rev 2: Updated max dump load value to 90 kW

Battery Model



Rev 2: Updated # of battery cells to 114

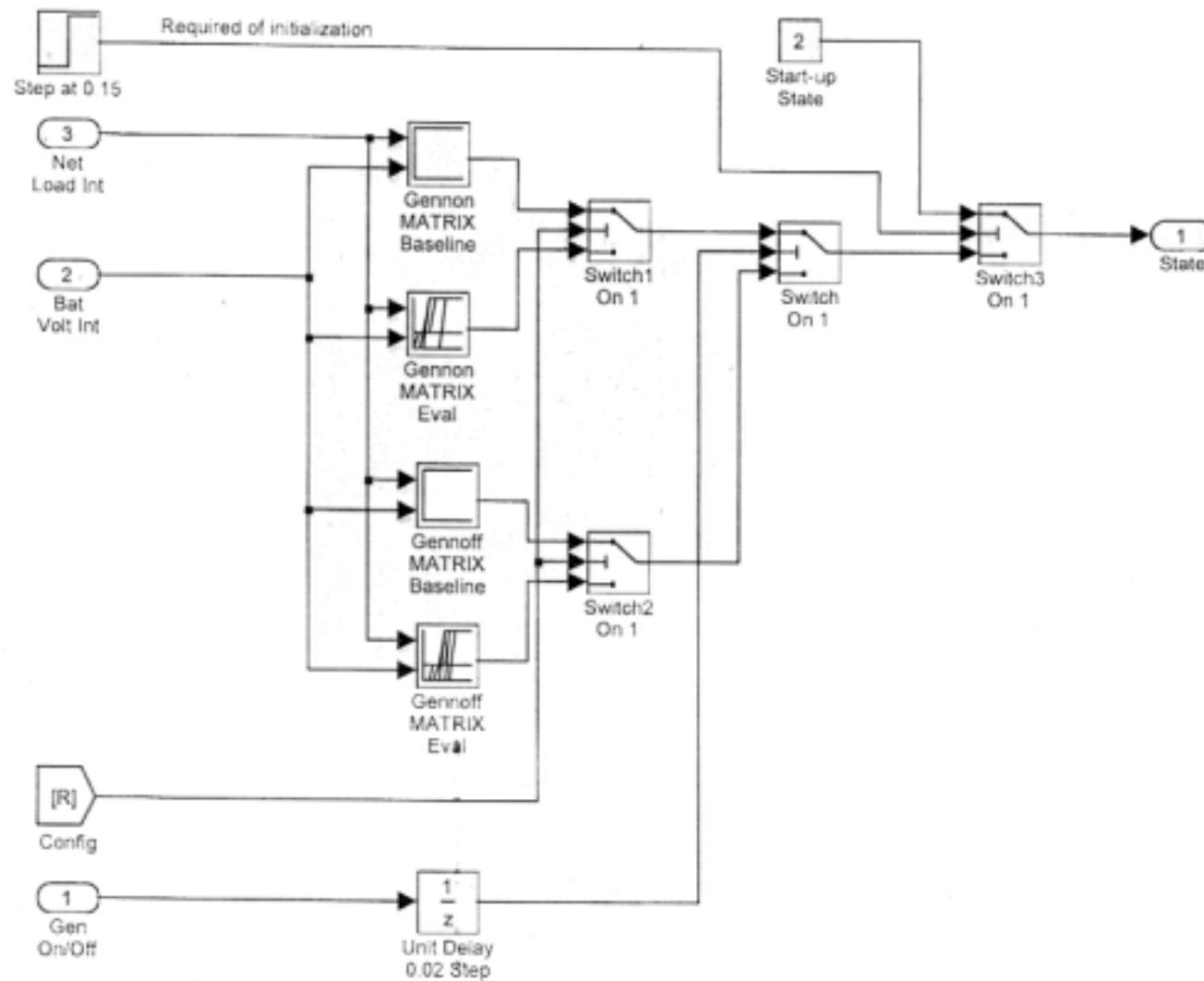
<u>V Look-Up Table</u>	
<u>In (Amp-hr)</u>	<u>Out (Volts)</u>
0	1.6
195	1.8
390	2.03
520	2.07
650	2.20
675	2.40
700	2.80



* NOTE: Negative output is defined as power out

Ver 3.0 Modified Model to remove dynamics to change time step to 1.0 = 1.0 hour. Improve run time.

Matrix Logic

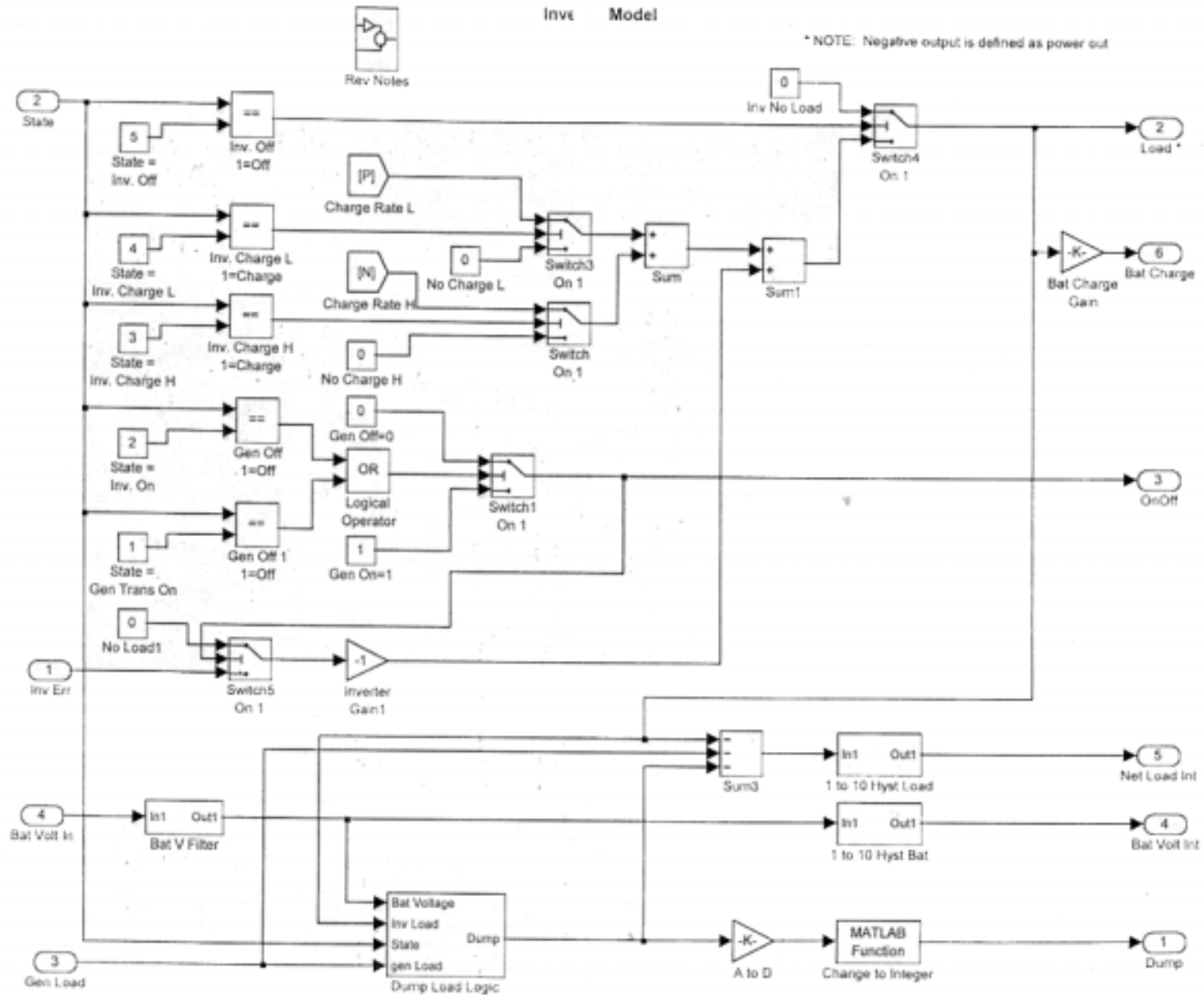


Rev 2: Added step function to force start-up in Inverter mode, Required due to Unit step delays in hyst function

Rev 2: Changed MATRIX Genon(1,3) from 3 to 2

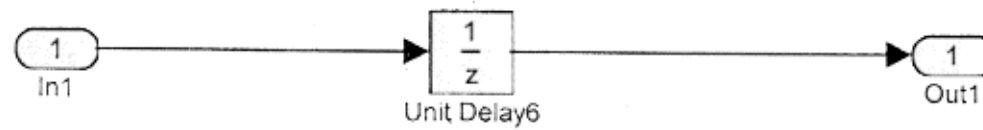
Ver 3.0 modified MATRIX tables to ref. MXBLON, MXBLOFF, MXEVON, and MXEVOFF

Rev 2: Change Net Load (row) saturation limits to 0 to 9 and update to new MATRIX tables



Bat V Filter

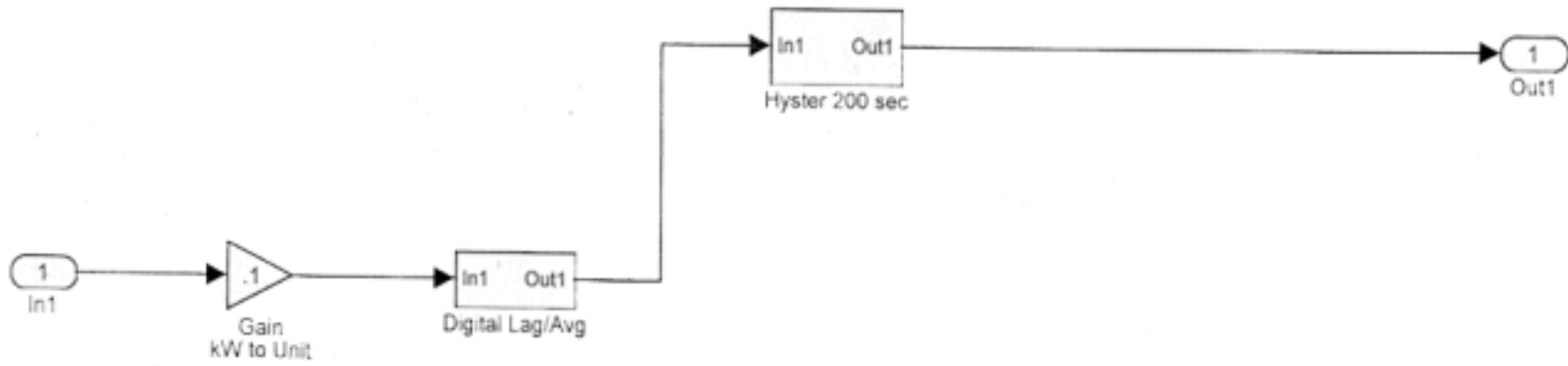
Delay to simulate dynamic filter



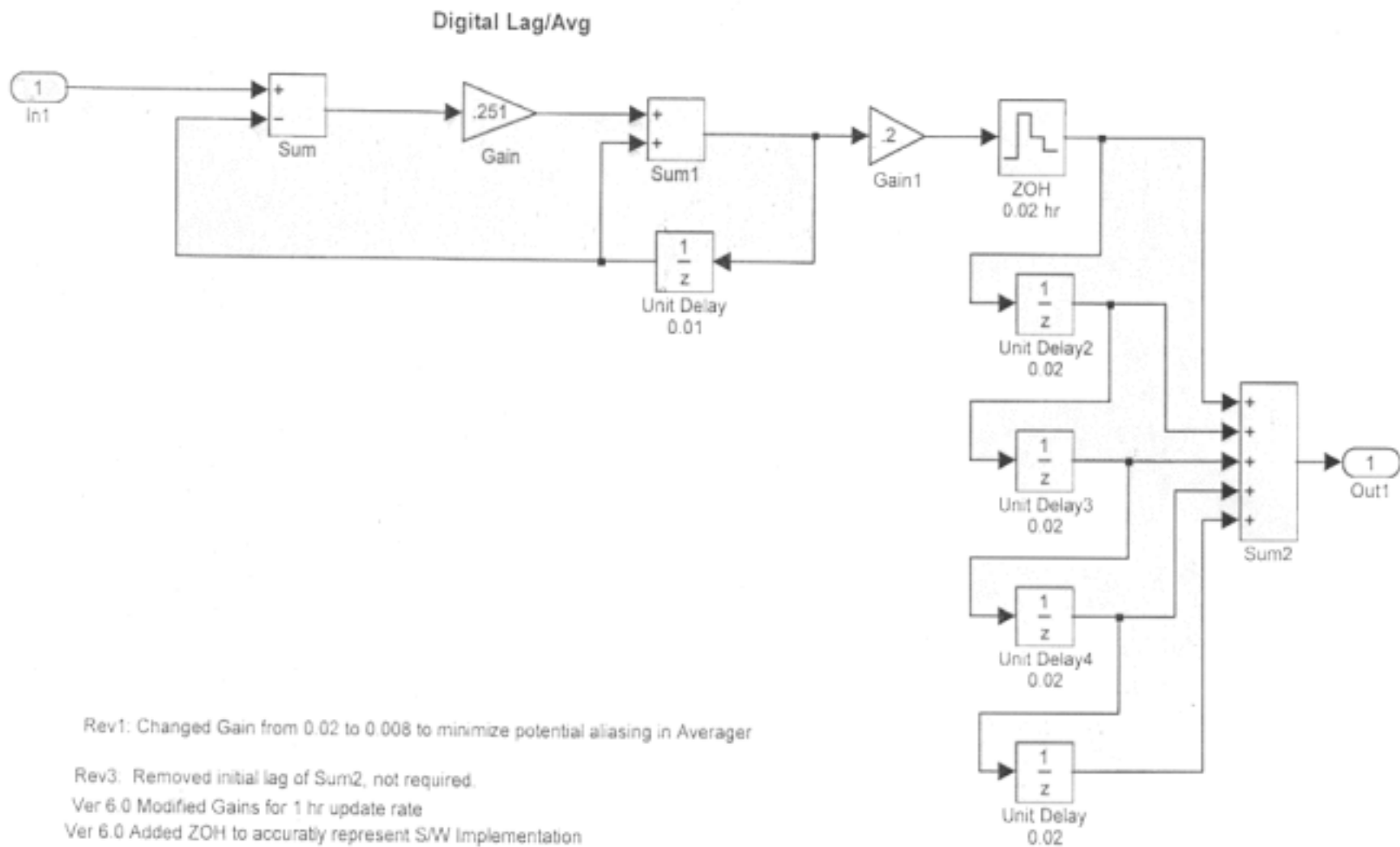
Delay Time = 0.02
Initial Cond = 230

Rev 2: Added battery filter

1 to 10 Hyst Load

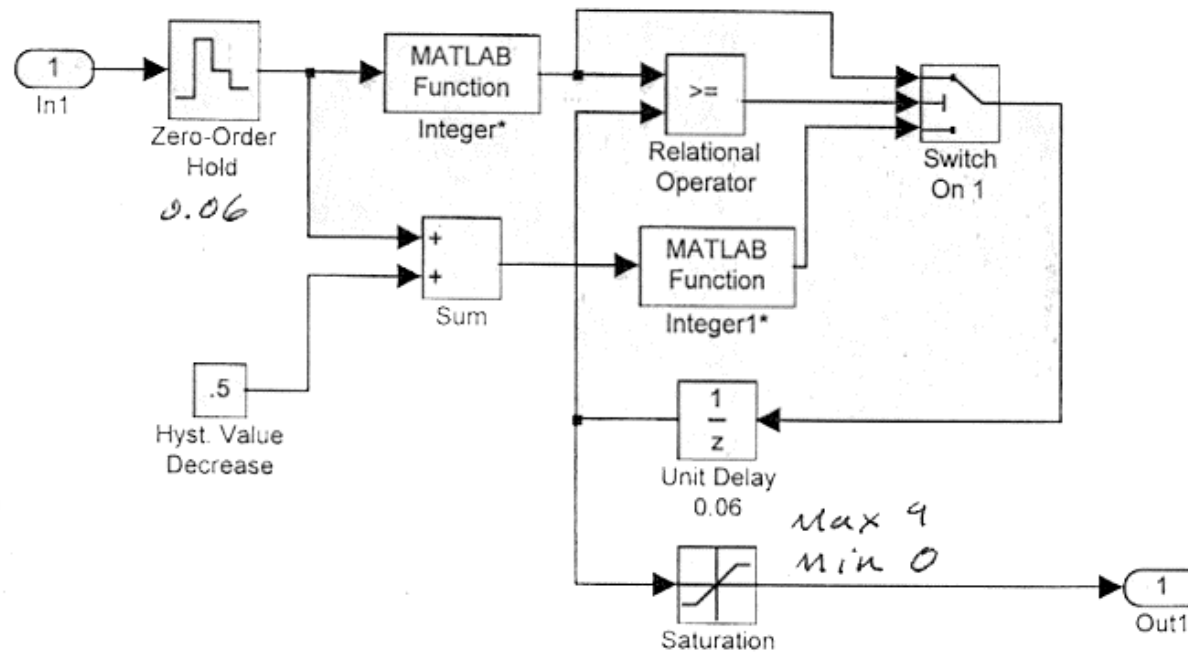


Rev 3: Changed First order lag (4 Step Lag) function to discrete implementation (Digital Lag)



Hyster 200 sec

(Float to Integer Conversion with hysteresis)



* NOTE: Float to Integer Conversion

Ver 3.0 Upated Hysteresis to a time step of 1.0 = 1.0 hr

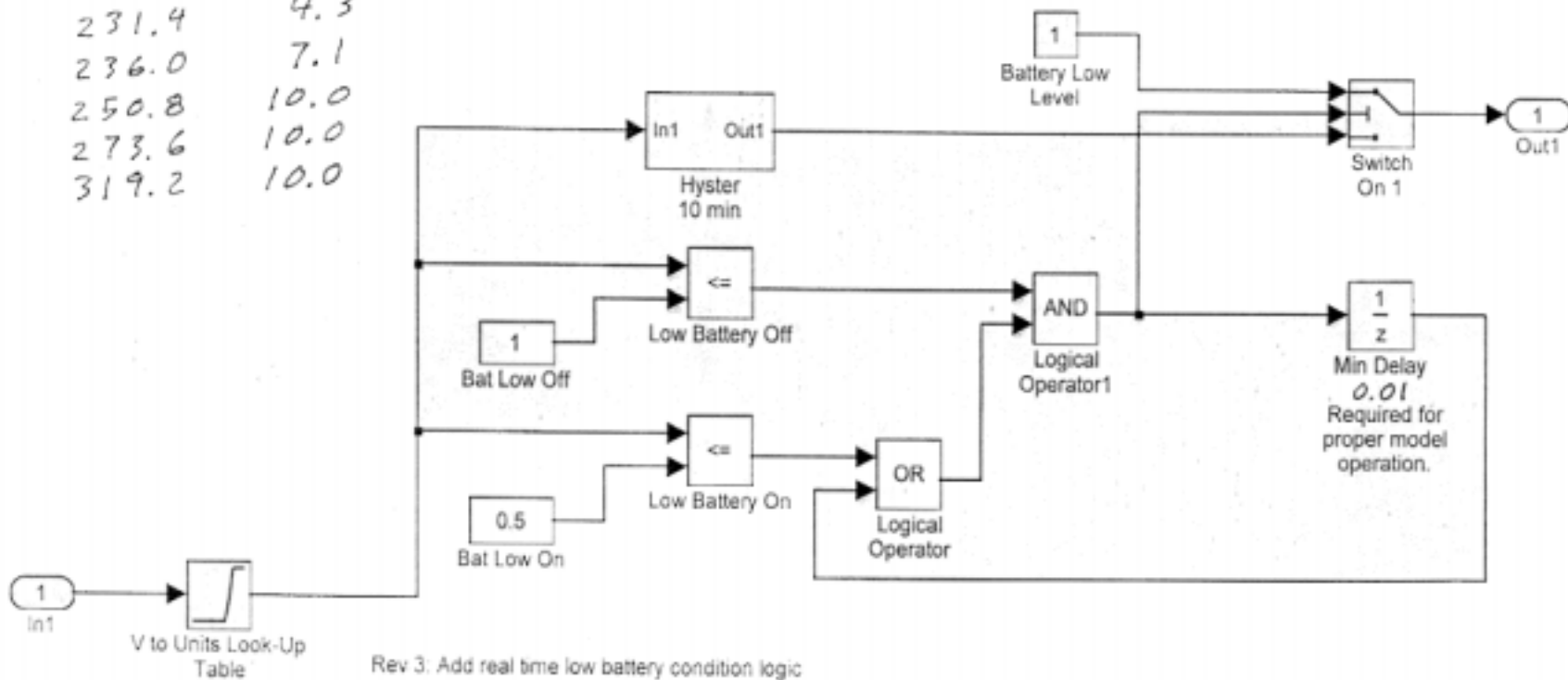
Rev 2: Change Net Load saturation limits to 0 to 9

Ver 6.0 Changed load delay to 200 sec ZOH

V to Units Look-up Table

In (Volts)	Out (SOC/10)
182.4	0.0
205.2	0.0
231.4	4.3
236.0	7.1
250.8	10.0
273.6	10.0
319.2	10.0

1 to 10 Hyst Bat

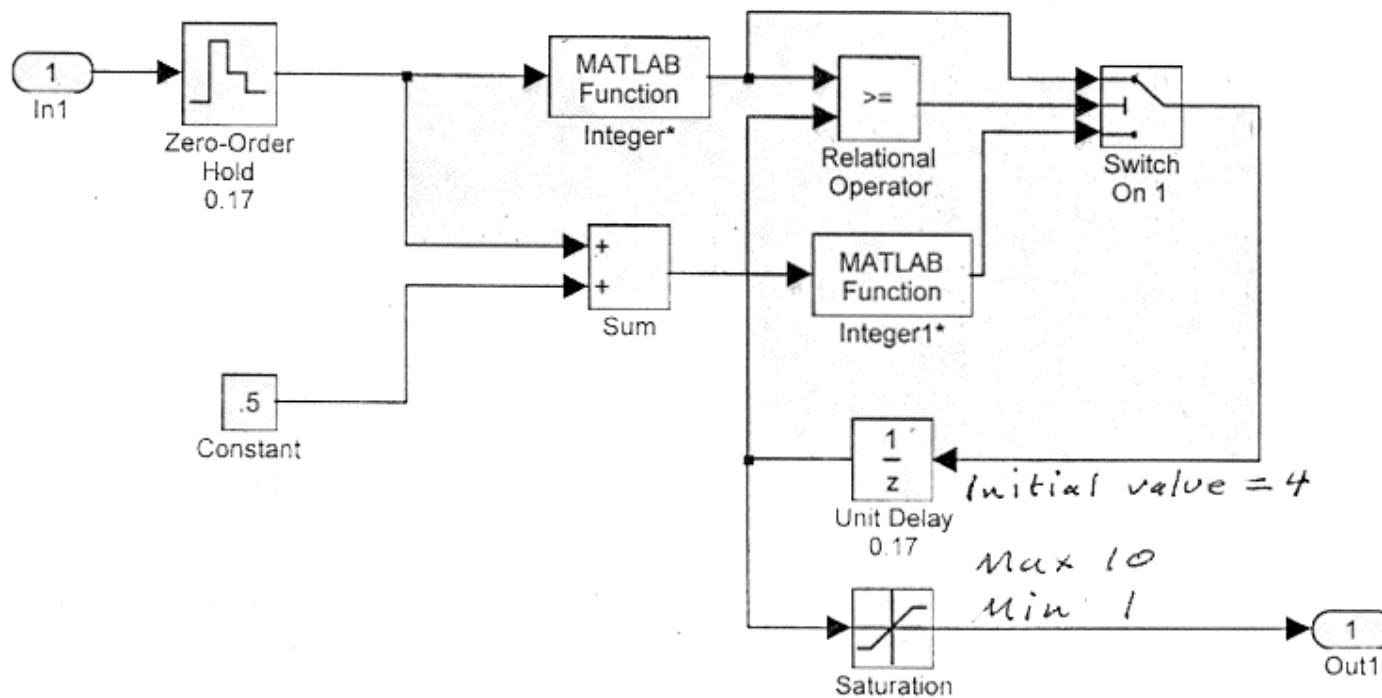


Rev 3: Add real time low battery condition logic

Rev 2: Updated the V to Units Look-up Table

Hyster 10 Min

(Float to Integer Conversion with hysteresis)

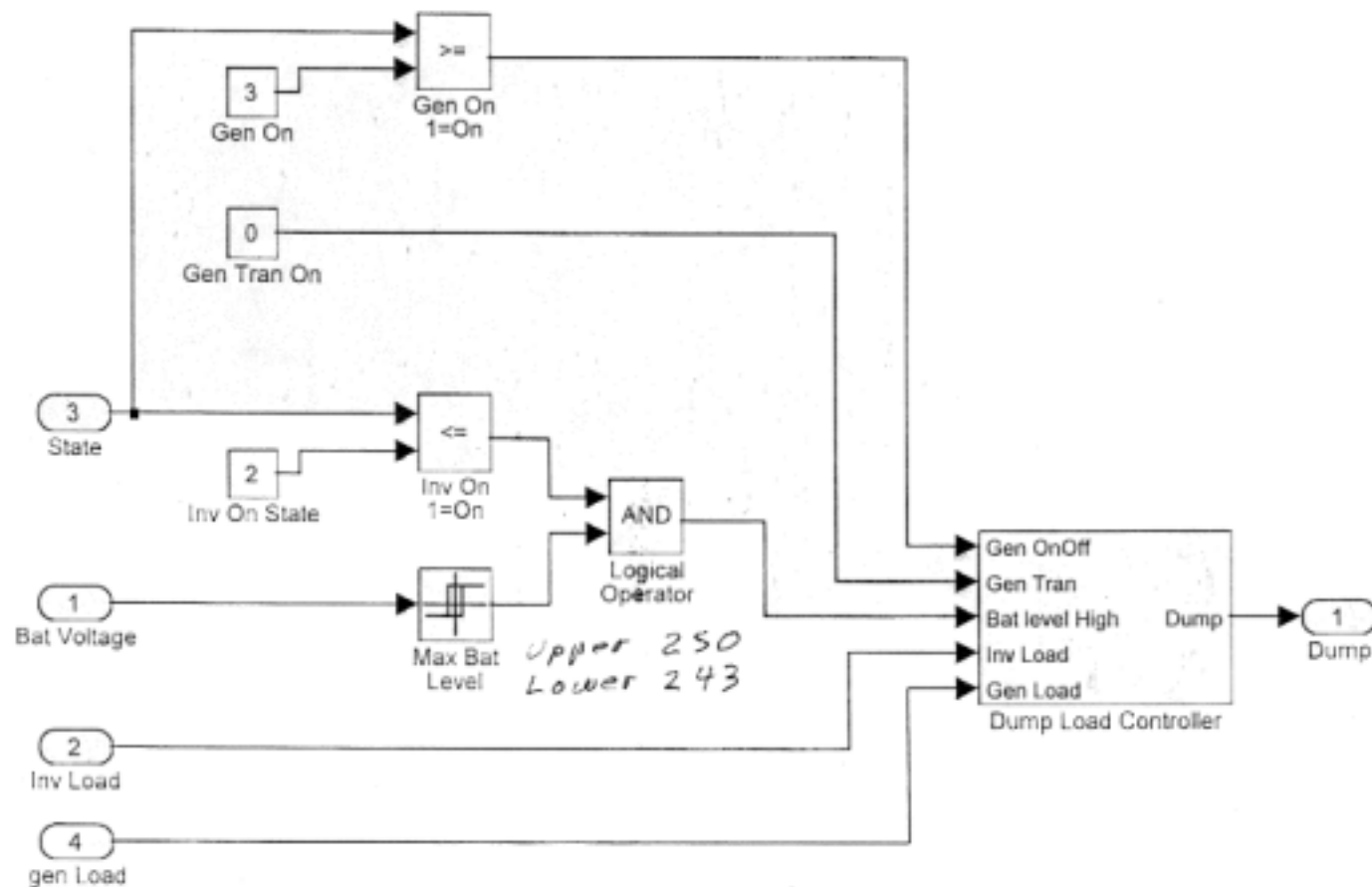


* NOTE: Float to Integer Conversion

Ver 3.0 Upated Hysteresis to a time step of 1.0 = 1.0 hr

Ver 6.0 Changed delay to 600 sec ZOH

Dump Load Logic



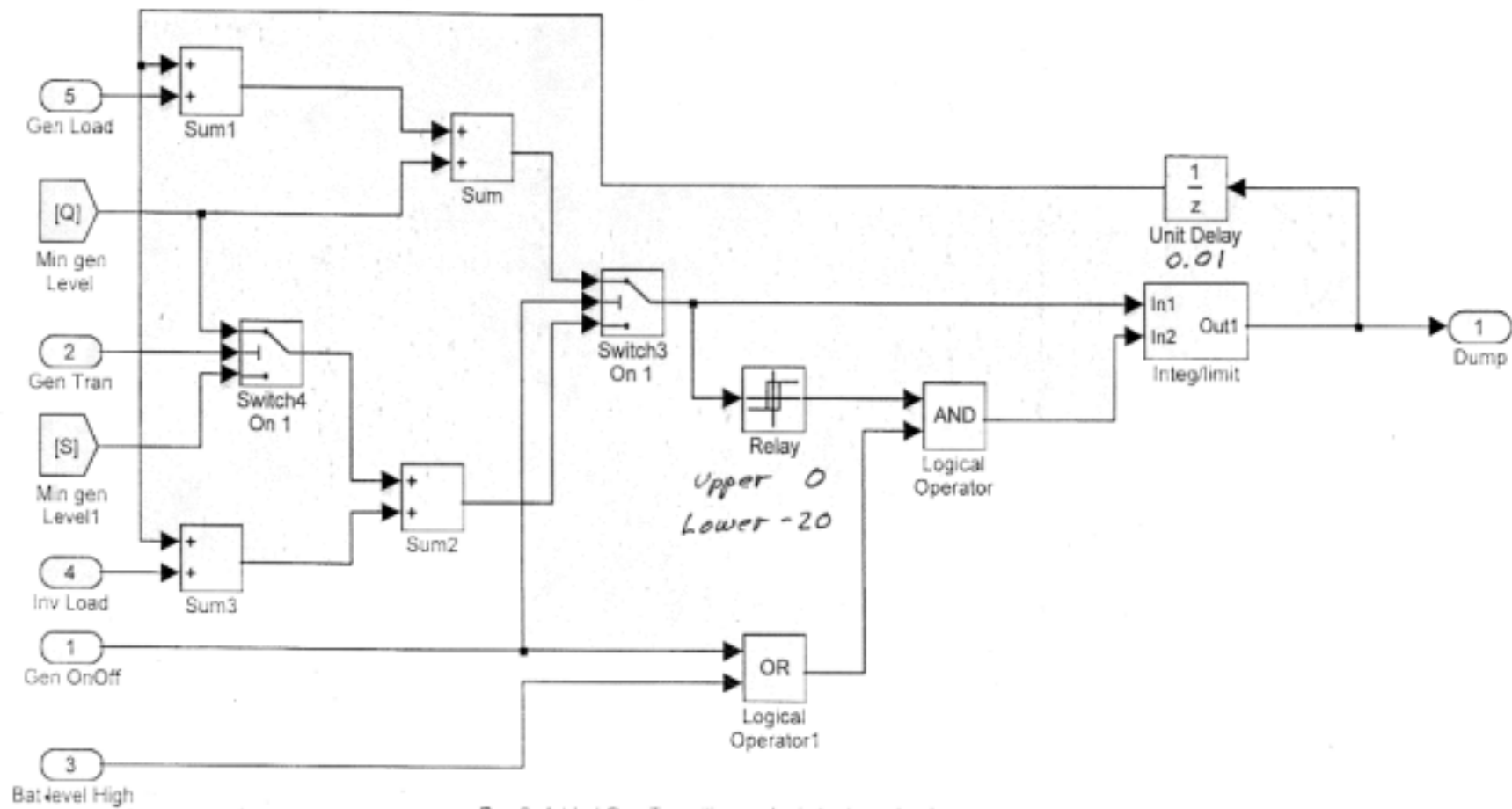
Ver 3.0 Modified Dump Logic to use Gen Load and Net Err. directly

Rev 2: Added Gen Transition on logic to dump load

Rev 2: Modify the Max Bat Level Hyst. values due to change in # of battery cells

Ver 6.0 Set Gen Tran to Off

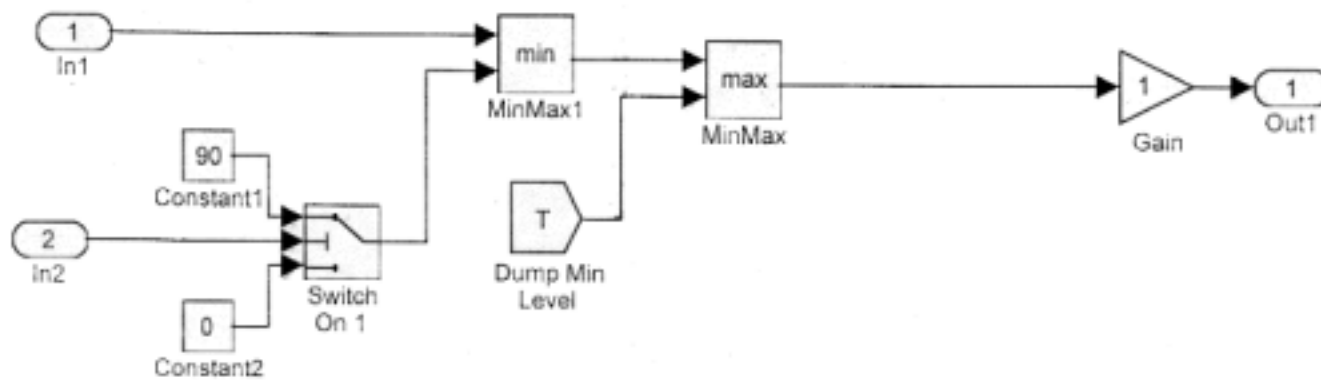
Dump Load Controller



Rev 2: Added Gen Transition on logic to dump load

Integ/Limit Function

(Designed to prevent Integrator wind-up)



Rev 3: Added min dump load value

Appendix C: Inverter Test Results

Functionality Checks

Before running the tests, functionality checks were conducted to verify proper inverter operation and state transition for steady- and quasi-steady-state operation. These checks verified that the system operated the way the hybrid controller intended it to and allowed any shortcomings to be noted. Although many of these checks had been performed on previous software revisions for the hybrid controller, these checks were necessary to benchmark the latest revision of the software code. Before starting the test, all inverter settings were confirmed on the inverter and recorded. Table 1 shows a listing of the inverter set points. Table 2 lists the functionality checks performed.

Table 1. Inverter Settings (Latest Code revision is Tag File rev 13)

Parameter Name*	Value	Units	Description
gen_warmup_time	15	sec	Generator warm-up time during start-up
MAX_BAT_HIGH	265	VDC	Max battery voltage for turning ON min dump load
MAX_BAT_LOW	257	VDC	Min battery voltage for turning OFF min dump load
MAX_ERR_DUMP_OF	-20	units	Inv/gen load level at which the dump function is
F			turned OFF
DUMP_INC_GAIN	50	units	Dump load integrator increase error gain
DUMP_DECR_GAIN	30	units	Dump load integrator decrease error gain
GEN_DUMP_MIN	15	kW	Trickle charge level after Max Bat High Voltage was
			reached
INV_DUMP_MIN	35	kW	Inverter min load level when battery is fully charged
DUMP_RATE_MAX	30	kW/sec	Dump load max rate of change
DUMP_RATE_MIN	30	kW/sec	Dump load min rate of change
DUMP_PERR_MAX	10	kW	Dump load proportional error offset
DUMP_PERR_GAIN	30	units	Dump load proportional error gain
DUMP_IERR_MIN	0	Kw	Dump load min setting

*Parameter name may not imply the function, as in the case of GEN_DUMP_MIN.

Table 2. Functionality Checks Performed

Functionality Check	HCU State	Description
Generator Min Load	Shutdown and Charge	Verify generator minimum load is 10 kW when village load is taken off system, add load back in 2-kW increments, and verify that min load = 10 kW
<i>Result:</i> Function confirmed		
State Transition from Inv. To Charge	Inv-Charge	Verify state transition with and without AC Source Sim running
<i>Result:</i> Transition confirmed both with and without AC Source Sim running		
State Transition from Charge to Inverter	Charge-Inv	Verify state transition with and without AC Source Sim running
<i>Result:</i> Transition confirmed both with and without AC Source Sim running		
Battery Charging Algorithm	Charge and Inv	Verify that battery-charging algorithm works with diesel and with AC Source Sim (i.e., diesel-on and diesel-off modes). Verify that dump load absorbs all excess power at Max Bat High setting above Gen Dump Min setting. Verify that hysteresis works and that batteries start charging when voltage drops below Max Bat Low (both diesel-on and diesel-off modes)
<i>Result:</i> Charging algorithm verified		
Dump Load	Inv	Verify that dump load absorbs all excess power when battery voltage is greater than Max Bat High and AC Source SIM is running
<i>Result:</i> Functionality of dump load verified		
Transition to Shutdown on Inverter Fault	Inv-Shutdown	In inverter mode, disconnect batteries (DC bus) and verify that inverter transitions to shutdown mode and that diesel starts and connects to village load
<i>Result:</i> Function verified		
Gen Dump Min	Inv	Verify that Gen Dump Min setting equals charging power to batteries when batteries are fully charged (i.e., trickle charge)
<i>Result:</i> Function verified		

1.1 Test Results with AC Source Simulator

The testing described in this section was conducted with the AC source simulator. The AC source simulator is a variable-speed drive that is connected to a nominal 60-kW induction generator that has a soft start connected in series. The test setup can be seen in Figure 5 in the main body of the report.

Note: All figures are “screen dumps” from the data acquisition system and as such, the units could not be put on the axis. The x-axis units are the time period in minutes, and the y-axis units are referenced in the figure title.

1.1.1. Test: Village Load Step Changes: Adding Load

Purpose: Determine the largest step load using the village load simulator that the system can handle both with and without the diesel generator and with and without the AC Source Simulator (AC SIM). Figure 6 is a time series plot demonstrating a typical load profile for this testing.

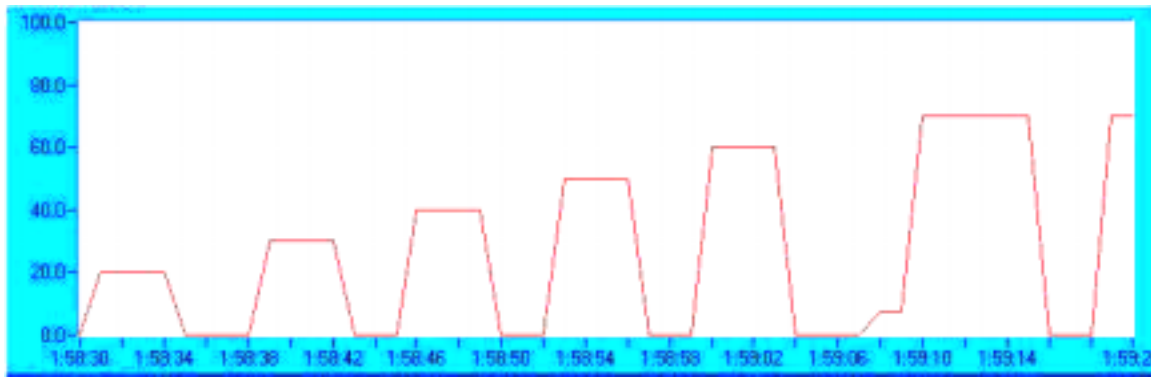


Figure 6. Village load (kW).

- Methodology:** Gen Only State: starting with a 0-kW Village Load (VL), increase the load stepwise on the VL to 20 kW. Repeat at 30, 40, 50, 60, and 70 kW as appropriate (stop incrementing load at first fault for tests 1-14). Repeat test with a VL power factor of 0.5.

Result: No faults to 70 kW. Same test results with the VL power factor set at 0.5.
- Methodology:** Repeat #1 in Charge State with AC SIM = 0 kW; up to 70 kW VL. Repeat test with a VL power factor of 0.5.

Result: No faults to 80 kW. With the power factor set at 0.5, there were no faults to 70 kW.
- Methodology:** Repeat #1 in Charge State with AC SIM = 10 kW; up to 80 kW VL. Repeat test with a VL power factor of 0.5.

Result: No faults to 80 kW. Tests began at 20 kW because it was the minimum stable village load. Same results with the VL power factor set at 0.5.
- Methodology:** Repeat #1 in Charge State with AC SIM = 56 kW; up to 100 kW VL. Repeat test with a VL power factor of 0.5.

Result: No faults to 60 kW. With a VL power factor at 0.5, the inverter was stable to 60 kW; it faulted at 80 kW due to low inverter frequency.

5. **Methodology:** Repeat #1 in Inverter State up to 100 kW w/no AC SIM. Repeat test with a VL power factor of 0.5.

Result: Fault at 60 kW because the inverter frequency was too low. With VL power factor at 0.5, the inverter was stable to 58 kW and then faulted because the inverter frequency was too low.

6. **Methodology:** Repeat #1 in Inverter State up to 100 kW w/no AC SIM. Repeat test with a VL power factor of 0.5.

Result: Fault at 100 kW, inverter frequency too low. System was able to function under an 80-kW load. With a VL power factor at 0.5, the inverter was stable to 60 kW; it faulted at 80 kW due to low inverter frequency.

7. **Methodology:** Repeat in Inverter State up to 100 kW with AC SIM = 65 kW. Repeat test with a VL power factor of 0.5.

Result: No faults to 100 kW. Same result with the VL power factor set at 0.5.

1.1.2 Test: Village Load Step Changes: Decreasing Load

Purpose: Determine the largest step load that the system can handle in both diesel-on and diesel-off modes (also with and without the AC SIM). Figure 7 shows a time series plot demonstrating a typical decreasing load pattern used during the tests.

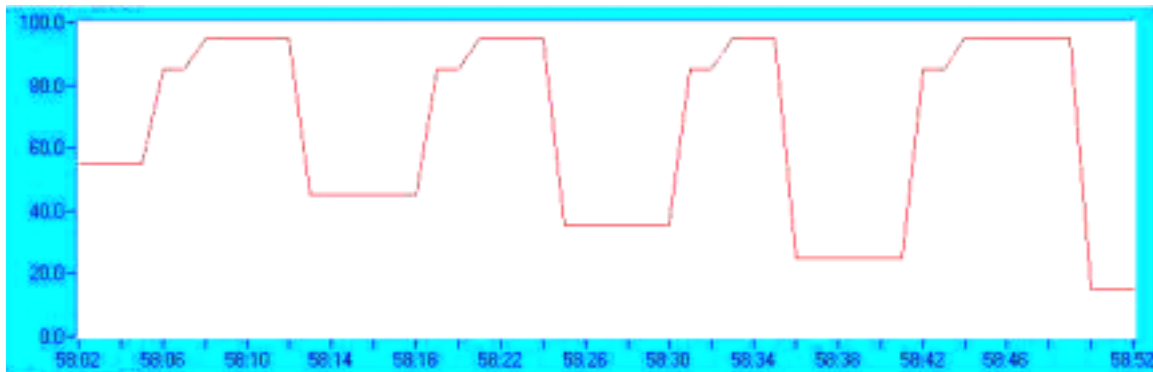


Figure 7. Village load (kW).

1. **Methodology:** Gen Only State: starting with a 75-kW VL, put a step load decrease on the VL of 20 kW. Repeat at 30, 40, 50, 60, and 70 kW as appropriate (stop decreasing load at first fault). Repeat test with a VL power factor of 0.5.

Result: No faults up to the 70-kW starting point. Same results with the VL power factor set at 0.5. 70 kW was the highest VL that the diesel generator could handle.

2. **Methodology:** Repeat #1 in Charge State with AC SIM = 0 kW; up to 70 kW VL. Repeat test with a VL power factor of 0.5.

Result: No faults to 70 kW. Same results with the VL power factor set at 0.5.

3. **Methodology:** Repeat #1 in Charge State with AC SIM = 10 kW; up to 90 kW VL. Repeat test with a VL power factor of 0.5.
Result: No faults to 90 kW. With VL power factor at 0.5, the inverter had no faults to 80 kW. At 80 kW, the inverter was unstable (high harmonic distortion in the current waveform).
4. **Methodology:** Repeat #1 in Charge State with AC SIM = 65 kW up to 100 kW VL. Repeat test with a VL power factor of 0.5.
Result: No faults to 100 kW. Same results with the VL power factor set at 0.5.
5. **Methodology:** Repeat #1 in Inverter State up to 100 kW w/no AC SIM and up to 100 kW, starting the VL at 95 kW. Repeat test with a VL power factor of 0.5.
Result: This test was completed with the modification of the VL starting power. The inverter faulted if the test began with a VL higher than 50 kW. With a VL starting power of 50 kW, there were no faults.
6. **Methodology:** Repeat in Inverter State up to 100 kW with AC SIM = 10 kW, starting the VL at 95 kW. Repeat test with a VL power factor of 0.5.
Result: This test was completed up to a 50-kW starting point. That was the maximum VL starting point that the system could handle. The AC SIM was unstable but oscillated around 10 kW. With the power factor at 0.5, the AC SIM was not stable enough to complete the test.
7. **Methodology:** Repeat in Inverter State up to 100 kW with AC SIM = 65 kW starting the VL at 95 kW. Repeat test with a VL power factor of 0.5.
Result: No faults to 100 kW.

1.1.3 Test: Wind Turbine Trip Offline: Diesel Generator On

Purpose: Determine the system stability, including dump load response, when an induction wind turbine contactor opens at near rated wind turbine power with the diesel generator online.

1. **Methodology:** Charge State. With AC SIM = 65 kW, batteries at low state of charge, diesel generator = about 40 kW, VL = 75 kW (this should be the max load the diesel generators can handle) @ PF = 1.0, open the wind turbine contactor and record response. Vary system settings as required to characterize system response. Verify dump load response.
Result: After the contactor was opened, the diesel generator output increased to 78 kW to meet the village load. Dump load never came on during the tests. No faults during the test.
2. **Methodology:** Charge State. With AC SIM = 65 kW and batteries at high state of charge, diesel generator = 10 kW (before transition to Inverter State) and DL making up the rest of power balance at VL = 0 kW and PF = 1.0, open the wind turbine contactor and record response. Vary system settings as required to characterize system response, repeating with VL = 5 kW.
Result: Tested with both a 0-kW village load and a 5-kW village load. The inverter was able to handle the wind turbine dropping off the grid for both tests. When the turbine dropped off the grid, the dump load turned off. There were no faults during this test.

1.1.4 Test: Wind Turbine Trip Offline: Diesel Generator Off

Purpose: Determine the system stability, including dump load response, when an induction wind turbine contactor opens at near rated wind turbine power with the diesel generator offline.

- Methodology:** Inverter State. With AC SIM = 65 kW and VL = 90 kW at PF = 1.0 and batteries at low state of charge, open the wind turbine contactor and record response. Vary system settings as required to characterize system response. Try test with lower PF on VL. Repeat test with VL at 5 kW.

Result: Inverter faulted at village loads of 5, 50, and 60 kW (power factor of 1). With the diesel generator off, the batteries need to pick up the load; however, they were unable to support the change in load while at a low state of charge.
- Methodology:** Inverter State. With AC SIM = 65 kW and VL = 80 kW at PF = 1.0 and batteries at high state of charge, open the wind turbine contactor and record response. Vary system settings as required to characterize system response. Repeat test with lower PF on VL. Repeat test with VL at 5 kW.

Result: Inverter faulted at village loads of 60 and 80 kW with power factors of both 1 and 0.5. With a VL of 5 kW, the inverter didn't fault.

1.1.5 Test: Battery Charging

Purpose: Verify battery charging algorithm at Max Bat High and Low set points and at Inv Dump Min and Gen Dump Min levels.

Background: The set points associated with the battery charging algorithm are Max Batt High, Max Batt Low, Inv Dump Min, and Gen Dump Min. In the inverter state, the charging algorithm allows the batteries to be charged at any charging rate until the battery bank reaches Max Batt High. Once the battery voltage reaches the Max Batt High set point (in this case, 265 volts), the dump load comes on, taking a percentage of the available charging power. The percentage of power dumped is determined by Max Batt Low, Inv Dump Min, and Gen Dump Min.

In the charge state, the batteries are charged until a voltage set point is reached; then the charging rate tapers off. The set point name is Battery Charging Voltage. The diesel-charging algorithm also incorporates a set point called the Battery Maximum Charging Current, which sets a limit on the battery charging current. This set point protects the batteries from charging at too great a charging rate.

- Methodology:** Verify that battery charging algorithm works with the AC SIM and the diesel generator. Verify that dump load absorbs all excess power at Max Bat High above Gen Dump Min Setting. Verify that hysteresis works and that batteries start charging when voltage drops below Max Bat Low (in both diesel-on and diesel-off modes) and no greater than the Inv. Dump Min Level.

Result: The battery charging algorithm worked per the control algorithm specification. The following charging and discharging processes were confirmed. 1) When the battery voltage reached the battery max depth of discharge voltage setting, the inverter shut down. 2) The battery charging algorithm was also confirmed. 3) The diesel charging algorithm was also verified.

Figures 8- 13 show time series plots for the testing. The setting during the following test diagrams are Max Batt High 265 volts, Max Batt Low 255 volts, Gen Dump Min 10 kW, and Inv Dump Min at 90 kw.

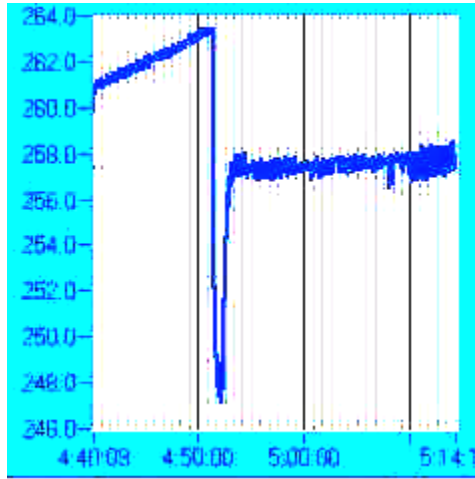


Figure 8. Battery voltage (V).

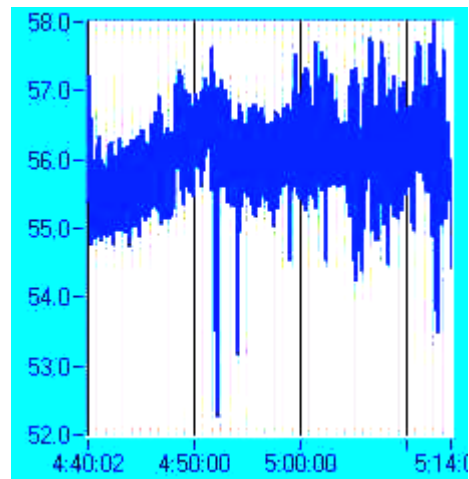


Figure 9. Village load (kW).

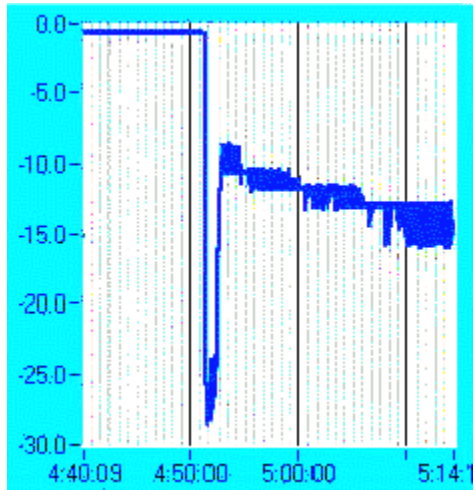


Figure 10. AC SIM power (kW).

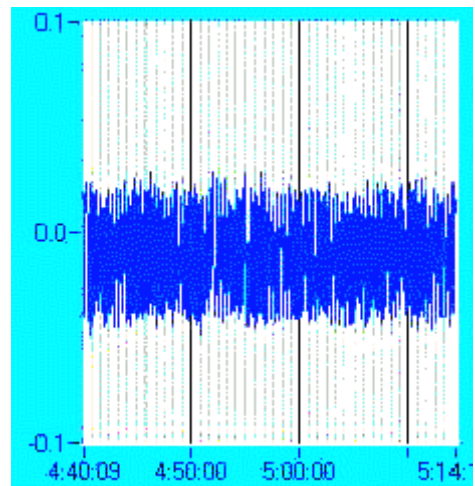


Figure 11. Genset power (kW).

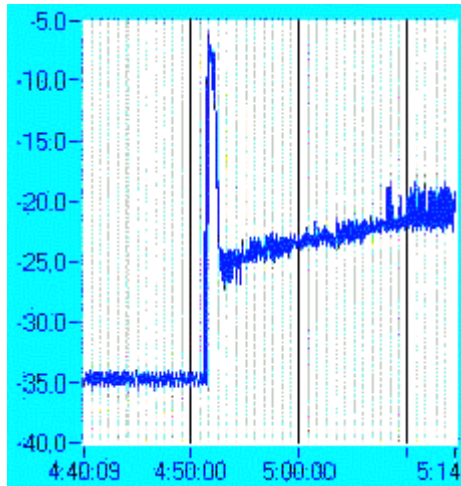


Figure 12. Inverter power (kW).

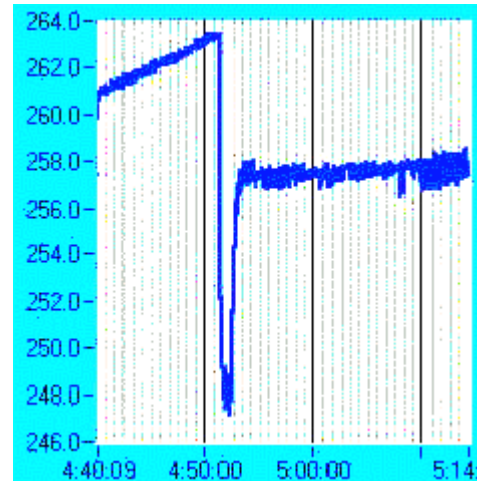


Figure 13. Dump load power (kW).

1.1.6 Test: State Transition from Inverter to Charge and from Charge to Inverter

Purpose: Verify state transition with and without AC Source Simulator running.

1. **Methodology:** Take time series plot of state transition Inverter to Charge and from Charge to Inverter with and without AC SIM.
Result: Figures 14-19 show time series plots of state transitions without the AC SIM running. The first transition shows the beginning of the test when the AC SIM is shut down and the inverter is put in inverter state. The next transition is from inverter state to charge state, followed by charge state to inverter state. At the end of the test, the AC SIM was turned on for the following tests with the AC SIM on:

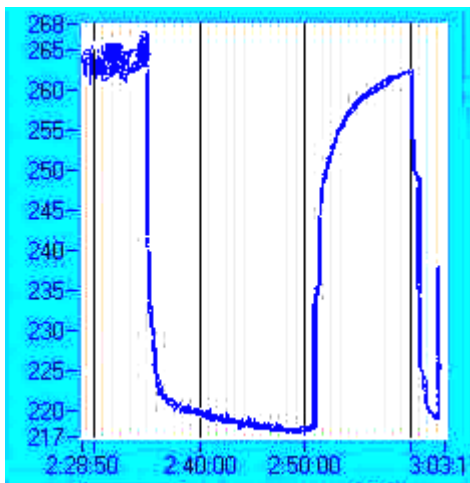


Figure 14. Battery voltage (V).

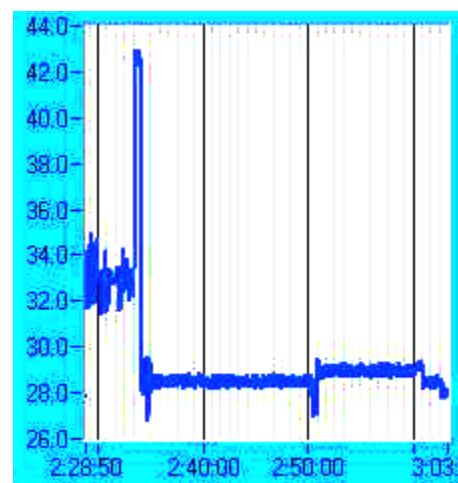


Figure 15. Village load (kW).

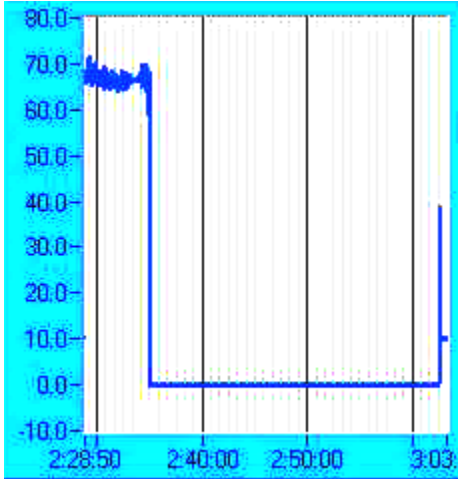


Figure 16. AC SIM power (kW).

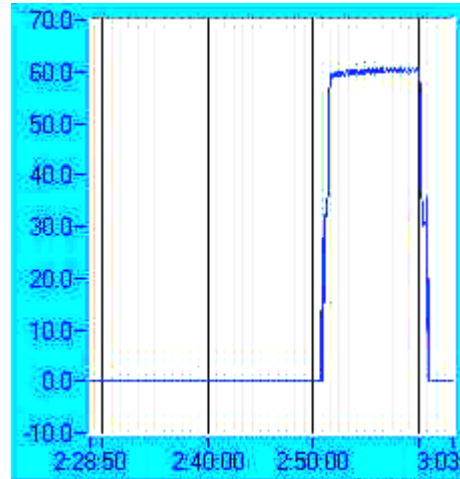


Figure 17. Genset power (kW).

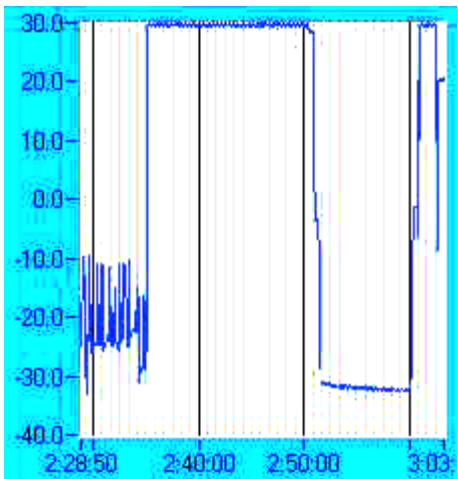


Figure 18. Inverter power (kW).

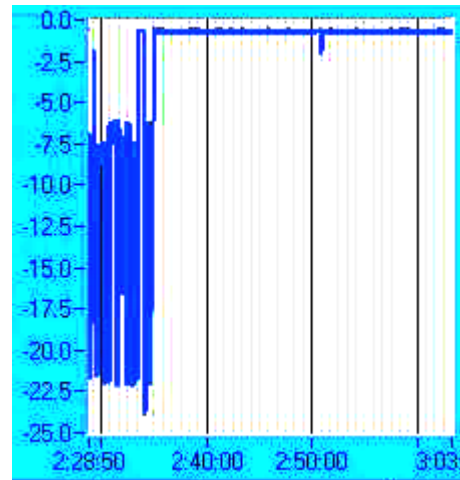


Figure 19. Dump load power (kW).

Figures 20-25 show time series plots of the tests with the AC SIM running. The tests began at the 40.00-min time mark when the inverter was put into inverter state. The following transition shows the inverter going into charge state. The next transition shows the inverter coming out of charge state and into inverter state. The continued increase in voltage is due to the AC SIM continuing to charge the batteries in inverter state.

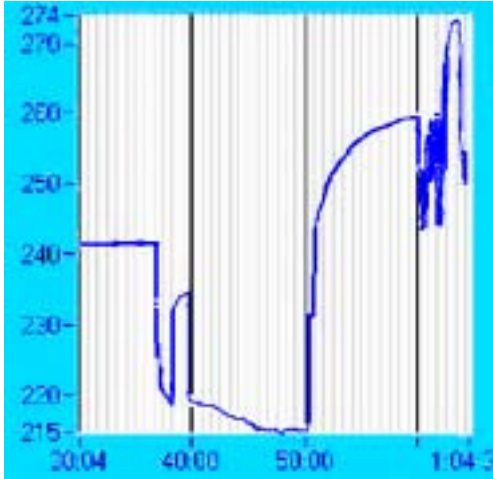


Figure 20. DC bus voltage (V).

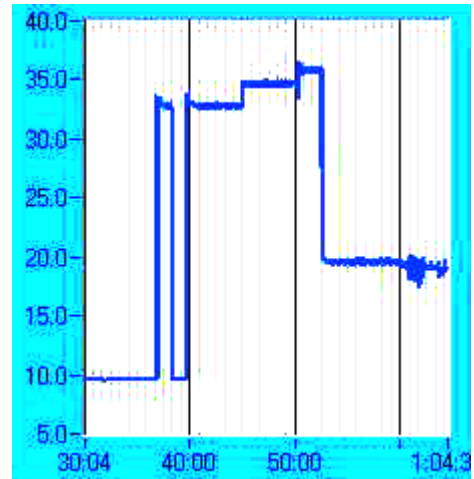


Figure 21. Village load (kW).

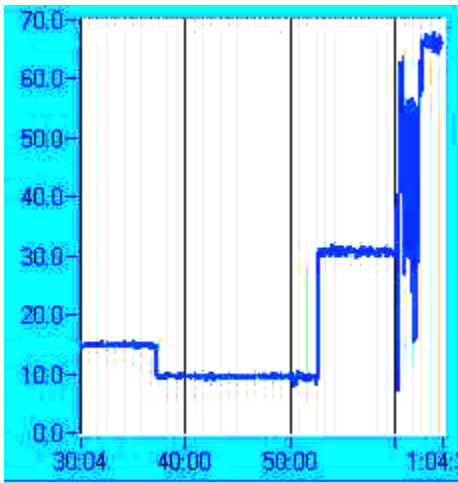


Figure 22. AC SIM power (kW).

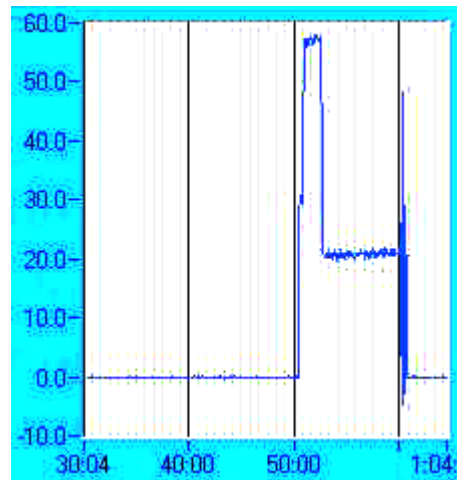


Figure 23. Genset power (kW).

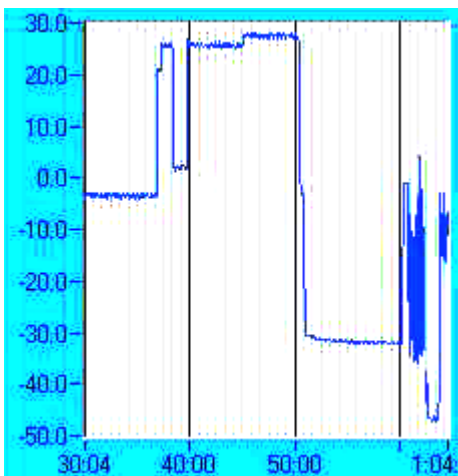


Figure 24. Inverter power (kW).

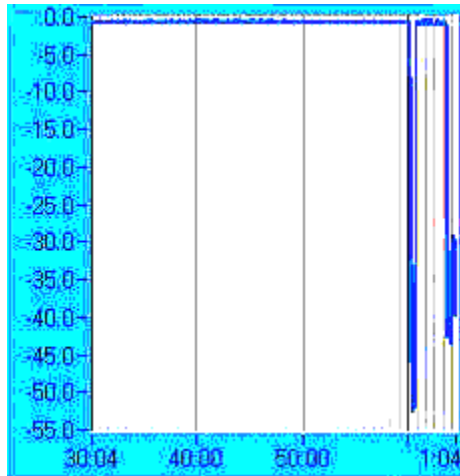


Figure 25. Dump load power (kW).

1.1.7 Test: Transition to Shutdown on Inverter Fault

Purpose: Verify Gen Only State on inverter fault.

1. **Methodology:** In inverter state, disconnect batteries (DC bus) and verify that inverter transitions to Gen Only State and that diesel generator starts and connects to village load.
Result: This transition was verified. When the batteries were disconnected, the inverter went to Gen Only State and the generator came on.

1.2 Testing with the AOC 15/50 Wind Turbine

1.2.1 Test: Wind Turbine Startup at High Power with Diesel

Purpose: Characterize system response to a high wind startup. **Note:** The AC SIM could not be used for this test or the following three tests. The AC SIM ramp up to high power production is too slow and therefore cannot characterize a high power. The AOC wind turbine was used, and as a result, these tests were dependent on ambient conditions (hence the variation in startup power).

1. **Methodology:** Charge State. Start AOC on diesel grid, batteries at low state of charge, diesel generator = about 10 kW, VL= 5 kW @ PF= 1.0. Vary system settings as required to characterize system response.
Result: AOC contactor closed with an initial power output of 38 kW. The dump load came on with the AOC and took most of the AOC output power. The diesel generator ran unsteadily at low power. No faults during testing.
2. **Methodology:** Charge State. Start AOC on diesel grid, batteries at low state of charge, diesel generator = about 75 kW, VL= 60 kW @ PF= 1.0. Vary system settings as required to characterize system response.
Result: AOC contactor closed with an initial power output of 40 kW. No faults.
3. **Methodology:** Charge State. Start AOC on diesel grid, batteries at high state of charge and dump load absorbing power, diesel generator = about 10 kW, VL= 5 kW @ PF= 1.0. Vary system settings as required to characterize system response. Verify dump load response.
Result: The AOC contactor closed at 53 kW. The dump load was active before and after the contactor closed. The system response was that the diesel generator unloaded and ran unsteady with output fluctuating between 5 and 13 kW.
4. **Methodology:** Charge State. Start AOC on diesel grid, batteries at high state of charge and dump load absorbing power, diesel generator = about 75 kW, VL= 60 kW @ PF= 1.0. Vary system settings as required to characterize system response.
Result: The AOC contactor closed at 44 kW. There was no dump load prior to contactor closing or after the contactor closed. The system response to the contactor closing was the diesel generator unloaded to 40 kW.

1.2.2 AOC 15/50 Soft Start Mode Start Up

Purpose: Verify that the AOC soft start is operational with the Xantrex inverter and that the inverter can bring the AOC on to the grid without faulting the inverter or overspeeding the turbine.

- Methodology:** Measure the voltage and current with an oscilloscope immediately after the AOC contactor has closed in order to verify that the soft start is operational. Confirm that the inverter does not fault and the AOC does not overspeed.
Result: Following in Figure 26 is the voltage and current on the startup. The scale is located in the bottom left corner of the plot. The AOC did not overspeed, and the inverter did not fault.

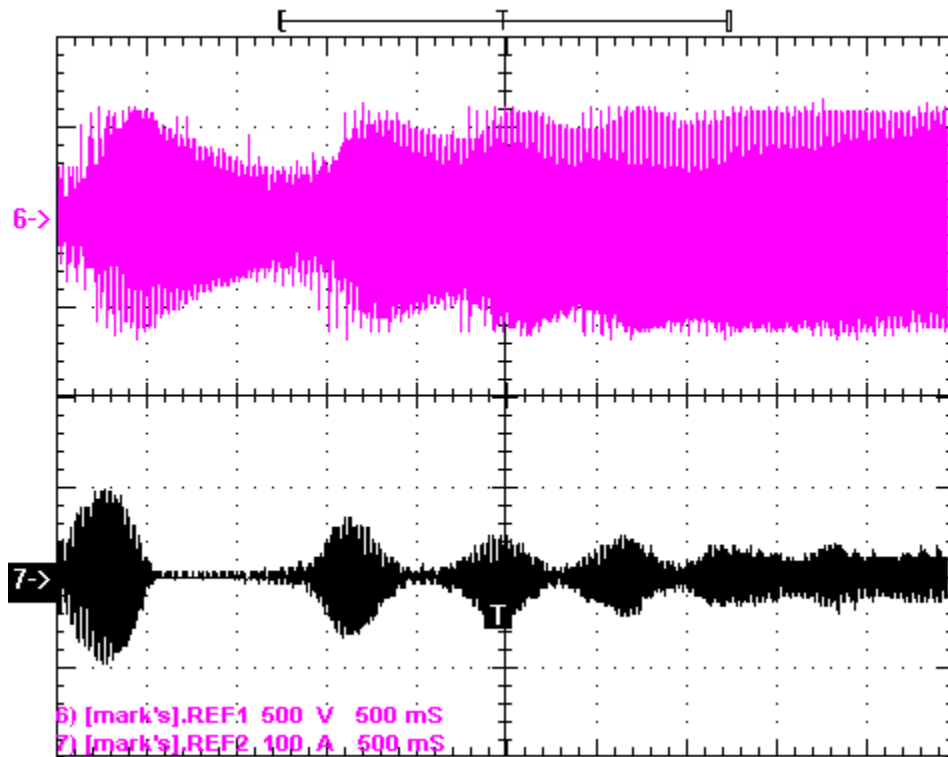


Figure 26. Oscilloscope reading of AOC startup.

Although the above test was performed successfully, it was not repeatable, and many times the AOC did not start successfully with the inverter but instead faulted on an overspeed condition. In order to rectify this situation, adjustments to the AOC soft start need to be made.

Once the AOC 15/50 turbine was online, the system would run without fault. Total run time with the AOC online was in excess of 80 hours, with good transitions between diesel-on and diesel-off modes.

Appendix D: A Preliminary Description of Parallel Operation of the Inverter with a Diesel Genset

The concept of limiting “max” generator output power on a hybrid inverter system has been implemented in prior projects by Xantrex with some success. The basic approach used an external device to the inverter to calculate the amount of current the inverter should discharge to limit the generator power. A separate controller was used because more information was available external to the inverter to help determine how much current the inverter should “source.”

When the inverter operates in the charge state and the sign of the current command is set opposite to the normal charge command, the inverter will discharge current to the grid. Although the mechanics of configuring the inverter to discharge current in the charge state are relatively simple, several issues must be addressed to ensure that the system functions properly. These issues are listed below.

- 1) Control stability of the limit loop is a major design factor. The dynamics of the inverter, generator, and overall grid must be considered when attempting to regulate a “fixed” generator power level; therefore, the system should be modeled to determine the response characteristics required and evaluate whether this can be achieved by the inverter. Trying to limit max generator power will also have a major impact on the design. If the design requirements are to minimize generator operation at high power, then a relatively simple control loop could be implemented. If the design requirements are to ensure the generator never exceeds a fixed limit, then a much more complex control logic would be required. Also, other issues must be considered with more stringent design requirements (see #3).
- 2) Logic would have to be included to ensure the inverter did not source power to the generator at low grid loads. Slow dynamics (for stability) may not respond fast enough during rapid drops in the grid load, resulting in the inverter sourcing current back into the generator.
- 3) The question of what to do when the battery is not charged sufficiently to support the required current demand must be addressed.
- 4) Maximum increasing and decreasing current ramp rates would have to be established to provide adequate stability while not limiting the response during rapid drops in grid power (see #2).

As described in the introductory notes, care should be taken to define the type and quantity of input signals required to control the amount of current the inverter should source. This may drive the design if the peak shave logic can be incorporated into the inverter or if a separate controller is required.

REPORT DOCUMENTATION PAGE			<i>Form Approved</i> OMB NO. 0704-0188	
Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.				
1. AGENCY USE ONLY (Leave blank)		2. REPORT DATE May 2003		3. REPORT TYPE AND DATES COVERED Technical Report
4. TITLE AND SUBTITLE Integration of Xantrex HY-100 Hybrid Inverter with an AC Induction Wind Turbine			5. FUNDING NUMBERS IG13.5000	
6. AUTHOR(S) D. Corbus, C. Newcomb, S. Friedly				
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) National Renewable Energy Laboratory 1617 Cole Blvd. Golden, CO 80401-3393			8. PERFORMING ORGANIZATION REPORT NUMBER NREL/TP-500-33445	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)			10. SPONSORING/MONITORING AGENCY REPORT NUMBER	
11. SUPPLEMENTARY NOTES				
12a. DISTRIBUTION/AVAILABILITY STATEMENT National Technical Information Service U.S. Department of Commerce 5285 Port Royal Road Springfield, VA 22161			12b. DISTRIBUTION CODE	
13. ABSTRACT (<i>Maximum 200 words</i>) Several issues must be addressed before solid-state inverters can be used in wind-diesel systems with larger wind turbines. This project addresses those issues by using a commercial hybrid inverter designed for PV-diesel systems and modifying the inverter for use with an AC induction wind turbine. Another approach would have entailed building an inverter specifically for use with an AC induction wind turbine, but that was beyond the scope of this project. The inverter chosen for this project was a Xantrex HY-100, an inverter designed for PV systems. The unit consists of an inverter/rectifier bridge, a generator interface contactor, a battery charge controller, a hybrid controller, and the associated control electronics. Details of the inverter may be found in Appendix A. A twofold approach was taken to integrating the existing inverter for use with an AC induction wind turbine: 1) development of a detailed model to model both steady-state and transient behavior of the system, and 2) modification and testing of the inverter with an induction wind turbine based on the modeling results. This report describes these two tasks.				
14. SUBJECT TERMS wind energy; wind turbines; wind-diesel systems; hybrid systems; solid-state inverters; AC induction wind turbine; Xantrex HY-100			15. NUMBER OF PAGES	
			16. PRICE CODE	
17. SECURITY CLASSIFICATION OF REPORT Unclassified	18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified	19. SECURITY CLASSIFICATION OF ABSTRACT Unclassified	20. LIMITATION OF ABSTRACT UL	